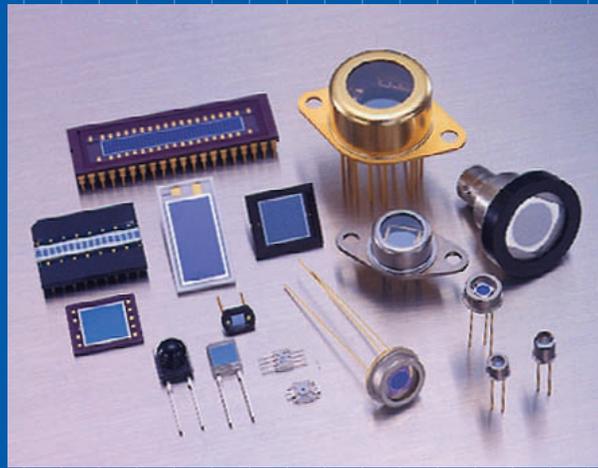


Si PHOTODIODE



HAMAMATSU

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Spectral response range (nm) 200 400 600 800 1000 1200	Feature	Application example	Type No.	Page
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Si photodiode for precision photometry and analytical instrument

190 ————— 1100	For UV to near IR range: UV sensitivity enhanced type	Spectrophotometer, analytical instrument environmental measurement, medical instrument	S1336/S1337 series etc.	1
190 ————— 1000	For UV to near IR range: UV sensitivity enhanced type (with suppressed IR sensitivity)		S1226/S1227 series etc.	2
320 ————— 1100	Visible to near IR range: IR sensitivity enhanced type	Copier, optical power meter, laboratory equipment, banking machine	S2386/S2387 series	3
	For excimer laser (193 nm) detection	Semiconductor production instrument	S8551, S8552, S8553, S9089	
	For monochromatic light (254 nm)	Analytical instrument, UV monitor	S2684-254, S9050	
380 ————— 780	For visible range	Photometric device, illuminometer	S9219 series, S7686	

Si photodiode for general photometry and camera application

320 ————— 840	For visible range	Camera application (exposure meter, illuminometer, auto strobe), light dimmer, copier	S1087, S5493-01, etc.	4
320 ————— 1100	For visible to near IR range	Copier, illuminometer, light dimmer	S4797-01, S1787-08, etc.	
400 ————— 720	For monochromatic light	White balance adjustment, color identification	S6428/S6429/S6430-01 S7505-01, S9032-02, etc.	5

Spectral response range (nm)	Feature	Application example	Type No.	Page	
					200

Si PIN photodiode

320	1000	Cut-off frequency: 500 MHz or more	Optical fiber communication, High-speed photometry	S8314, S5973-01, S9055, etc.	6
320	1060	Cut-off frequency: 100 MHz to less than 500 MHz		S8223, S5971, etc.	
320	1100	Cut-off frequency: 10 MHz to 100 MHz	Optical fiber communication, analytical instrument, optical power meter	S2506-02, S5106, etc.	8
320	1120	Large active area	For high energy physic	S3590-01, etc.	9
360	1120	For YAG laser detection	YAG laser detection, Analytical equipment, etc.	S3759	

Si photodiode array

190	1100	UV to near IR range: UV sensitivity enhanced type	Multichannel spectrophotometer, color analyzer	S4111/S4114 series, etc.	10
190	1100	Si PIN photodiode array (1)	Position detection, laser beam alignment	S2721-02, etc.	
320	1000	Si PIN photodiode array (2)	High-speed 2D photometry, 2D spec- trophotometry, 3D shape measurement	S7585, S3805	11
	760	1100	Incident light angle sensor	Incident angle detection of infrared LED and sunlight	

Si photodiode with preamp, TE-cooled type Si photodiode

190	1100	Si photodiode with preamp	Low-light-level measurement, NOx sensor	S9269, S9270, S9295 series S8745-01, S8746-01	12
320	1060	Si PIN Photodiode with preamp for optical fiber communication	Optical fiber communication, video signal transmission, optical disk pickup	S6468 series	
320	1060	Si PIN photodiode with preamp for spatial light transmission	Spatial light transmission	S7516 series	13
190	1100	TE-cooled type Si photodiode		S2592/S3477 series	

Si APD (avalanche photodiode)

400	1000	Low bias operation type	Spatial light transmission, Rangefind- er, Optical fiber communication	S2381 to S2385, etc.	14
		Low temperature coefficient type		S6045 series	
200	1000	Short wavelength type	Low-light-level measurement, analytical instrument	S5343, S5344, S5345 S8664 series, etc.	15
400	1100	Long wavelength type	YAG laser detection, Long wavelength light detection	S8890 series	
400	1000	Multi-element type	Low-light-level measurement, laser beam alignment	S4402	

X-ray detector

X-ray region from several ten keV to 100 keV	Photodiode coupled to high- sensitivity X-ray scintillator	Baggage inspection system, non- destructive inspection system	S8559, S8193, S5668 series, S7878	16
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Si photodiode for precision photometry and analytical instrument

Featuring high sensitivity and low dark current, these Si photodiodes are specifically designed for precision photometry in a wide range of fields.

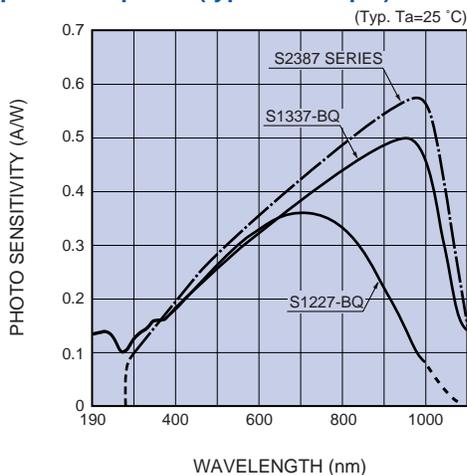
For UV to near IR range: UV sensitivity enhanced type

These Si photodiodes have sensitivity in the UV to near IR range. The BQ type delivers high sensitivity exceeding 0.1 A/W in the UV range. Other features include low dark current, low terminal capacitance and low noise, making these photodiodes ideal for precision photometry such as analytical instrument. The BU type is designed to provide enhanced reliability in detecting high power UV light such as from mercury lamps.

Type No.	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Active area (mm)	Dark current $V_R=10$ mV Max. (pA)	Package
S1336-18BU	190 to 1100	960	1.1 × 1.1	20	① TO-18
S1336-18BQ					
S1336-18BK	320 to 1100		2.4 × 2.4	30	② TO-5
S1336-5BQ	190 to 1100				
S1336-5BK	320 to 1100		3.6 × 3.6	50	③ TO-8
S1336-44BQ	190 to 1100				
S1336-44BK	320 to 1100		5.8 × 5.8	100	⑤ Ceramic
S1336-8BQ	190 to 1100				
S1336-8BK	320 to 1100		1.1 × 5.9	30	⑥ Ceramic
S1337-16BQ	190 to 1100				
S1337-16BR	320 to 1100		2.4 × 2.4	30	⑦ Ceramic
S1337-33BQ	190 to 1100				
S1337-33BR	320 to 1100		5.8 × 5.8	100	⑧ Ceramic
S1337-66BQ	190 to 1100				
S1337-66BR	320 to 1100		10 × 10	200	⑩ Ceramic
S1337-1010BQ	190 to 1100				
S1337-1010BR	320 to 1100		18 × 18	1000	⑨ Ceramic
S6337-01	190 to 1100				
S2551	320 to 1060	920	1.2 × 29.1	1000	⑪ With BNC connector
S2281 *	190 to 1100	960	φ11.3	500	⑫ With BNC connector
S2281-04 *			φ7.98		

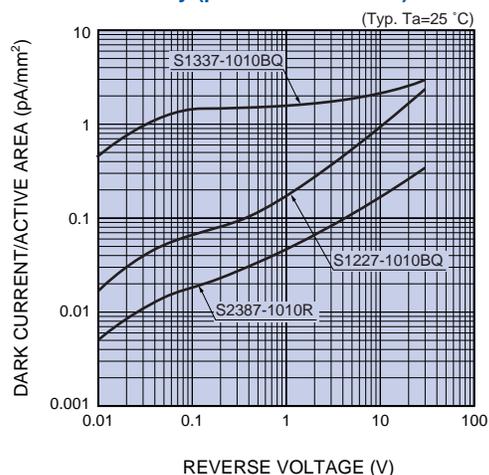
* When connected to C2719 photosensor amplifier (using E2573 BNC-BNC coaxial cable), low level photocurrent can be amplified with low noise.

■ Spectral response (typical example)



KSPDB0186EA

■ Dark current density (per unit active area) vs. reverse voltage



KSPDB0195EA

For UV to near IR range: UV sensitivity enhanced type (with suppressed IR sensitivity)

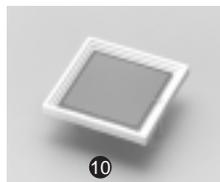
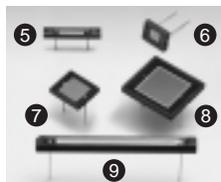
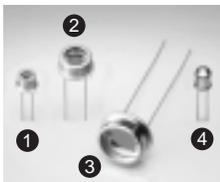
These Si photodiodes have suppressed IR sensitivity. The BQ type delivers high sensitivity exceeding 0.1 A/W in the UV range. Since the dark current is greatly reduced, these photodiodes are ideal for low-light-level detection. The BU type is designed to provide enhanced reliability in detecting high power UV light such as from mercury lamps.

Type No.	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Active area (mm)	Dark current VR=10 mV Max. (pA)	Package	
S1226-18BU S1226-18BQ	190 to 1000	720	1.1 × 1.1	2	①	TO-18
S1226-18BK	320 to 1000		2.4 × 2.4	5	②	TO-5
S1226-5BQ	190 to 1000					
S1226-5BK	320 to 1000					
S1226-44BQ	190 to 1000		3.6 × 3.6	10	③	TO-8
S1226-44BK	320 to 1000					
S1226-8BQ	190 to 1000		5.8 × 5.8	20	⑤	Ceramic
S1226-8BK	320 to 1000					
S1227-16BQ	190 to 1000		1.1 × 5.9	5	⑥	Ceramic
S1227-16BR	320 to 1000					
S1227-33BQ	190 to 1000		2.4 × 2.4	5	⑦	Ceramic
S1227-33BR	320 to 1000					
S1227-66BQ	190 to 1000		5.8 × 5.8	20	⑧	Ceramic
S1227-66BR	320 to 1000					
S1227-1010BQ	190 to 1000		10 × 10	50	⑨	Ceramic
S1227-1010BR	320 to 1000					
S2281-01	190 to 1000		φ11.3	300	⑩	With BNC connector

Visible to near IR range: IR sensitivity enhanced type

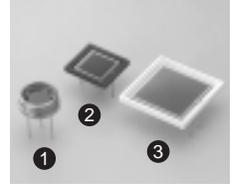
These Si photodiodes offer enhanced sensitivity especially in the near IR range. Low dark current and excellent linearity make these photodiodes suited for use in optical power meters and other photometric applications.

Type No.	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Active area (mm)	Dark current VR=10 mV Max. (pA)	Package	
S2386-18K	320 to 1100	960	1.1 × 1.1	2	①	TO-18
S2386-18L				2	④	
S2386-5K			2.4 × 2.4	5	②	TO-5
S2386-44K						
S2386-45K			3.9 × 4.6	30	③	TO-8
S2386-8K			5.8 × 5.8	50		
S2387-16R			1.1 × 5.9	5	⑤	Ceramic
S2387-33R						
S2387-66R			5.8 × 5.8	50	⑦	Ceramic
S2387-1010R						
S2387-130R			1.2 × 29.1	100	⑨	Ceramic



For excimer laser detection

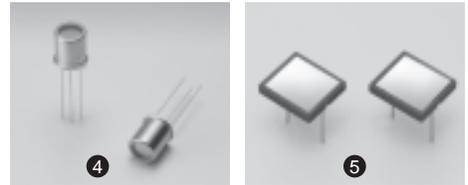
These Si photodiodes are specially optimized for excimer laser detection (ArF: 193 nm, KrF: 248 nm): sensitive in the vacuum UV (VUV) range. Compared to conventional types, these photodiodes exhibit little deterioration in sensitivity from VUV exposure, allowing stable measurement over long periods of time. S8551 is also available with a quartz glass window or MgF₂ window.



Type No.	Photo sensitivity $\lambda=193$ nm (A/W)	Active area (mm)	Dark current $V_R=10$ mV Max. (nA)	Package
S8551	0.06	5.8 × 5.8	0.5	① TO-8 (without window)
S9089 NEW		10 × 10	1.0	② TO-8
S8552		18 × 18	5.0	③ Ceramic (without window)
S8553				

For monochromatic light

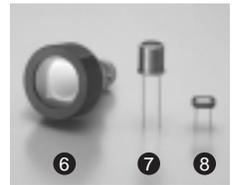
S2684-254 is highly sensitive only to monochromatic light using an interference filter. The spectral response width is as narrow as 10 nm (FWHM), allowing accurate measurement without effects from stray light. S2684-254 has its peak sensitivity at 254 nm Typ. Other types having the peak sensitivity at different wavelengths such as 340, 405, 500, 520, 560, 650 and 700 nm are also available upon request.



Type No.	Sensitivity wavelength spectral width (nm)	Peak sensitivity wavelength (nm)	Active area (mm)	Dark current $V_R=10$ mV Max. (pA)	Package
S2684-254	10	254	3.6 × 3.6	25	④ TO-5
S9050 NEW	20	322	5.83 × 5.83	0.1 (nA)	⑤ Ceramic

For visible range

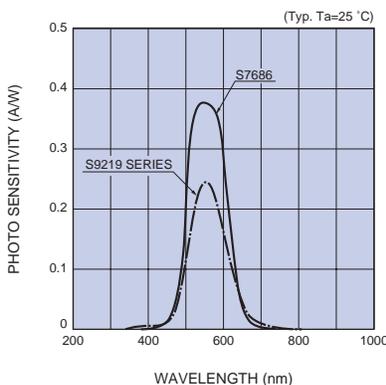
These Si photodiodes have a visual-compensated filter to provide spectral response characteristics similar to the human eye. S9219 is assembled in a metal package with a BNC connector.



Type No.	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Active area (mm)	Dark current $V_R=10$ mV Max. (pA)	Package
S9219 NEW	380 to 780	550	$\phi 11.3$	500	⑥ With BNC connector
S9219-01 NEW			3.6 × 3.6	50	⑦ TO-5
S7686			2.4 × 2.8	20 *	⑧ Ceramic

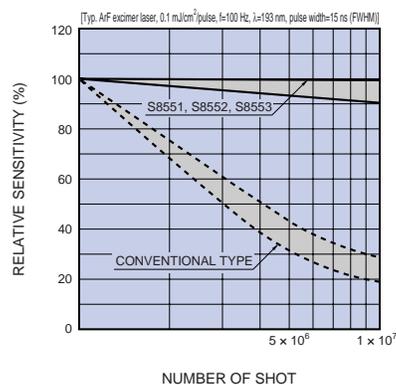
* $V_R=1$ V

■ Spectral response (S9219 series, S7686)



KSPDB0196EB

■ Variation in sensitivity due to UV exposure (S8551, S8552, S8553)



KSPDB0188EB

Si photodiode for general photometry and camera application

These Si photodiodes are used in various fields including general photometry and camera applications, featuring high sensitivity and low dark current. These are grouped into 3 types according to their spectral response characteristics: visible type, visible to near IR type and monochromatic type.

For visible range

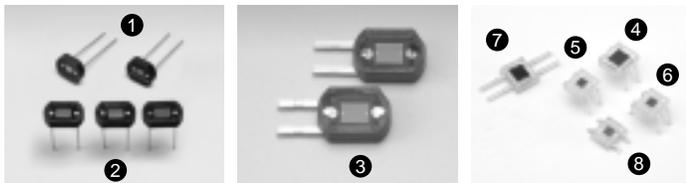
These Si photodiodes have sensitivity only in the visible range. S1087, S1133 and S1787-04 exhibit low dark current suitable for high precision measurement. S5493-01, S5627-01 and S7123-01/02 ensure high reliability since they do not use visual-compensated filters.

Type No.	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Active area (mm)	Dark current VR=1 V Max. (pA)	Package
S1087	320 to 730	560	1.3 × 1.3	10	①
S1133			2.4 × 2.8		②
S1787-04					③
S5493-01	320 to 840	540	2.4 × 2.8	100	④
S5627-01			1.3 × 1.3	50	⑤
S7123-01			2.46 × 2.46	100	④
S7123-02			2.4 × 2.8		②

For visible to near IR range

These Si photodiodes have sensitivity in the visible to near IR range. Their low dark current allows high precision measurement. S1133-14, S1787-12, S4797-01 and S6931 are designed to have low sensitivity in the near IR range.

Type No.	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Active area (mm)	Dark current VR=1 V Max. (pA)	Package	
S1787-12	320 to 1000	650	2.4 × 2.8	20	③	
S4797-01		720	1.3 × 1.3		⑥	
S6931			2.4 × 2.8		⑦	
S1133-14	320 to 1100	960	1.3 × 1.3	10	②	
S4011-04			2 × 2		⑧	
S6865-01					2.4 × 2.8	④
S1787-08			1.3 × 1.3			③
S2833-01						⑦
S1087-01			2.4 × 2.8		①	
S1133-01					②	
S6865-02					②	



For monochromatic light

S6428-01, S6429-01 and S6430-01 are monochromatic color sensors sensitive to blue, green and red light, respectively. S7505-01, S8751 and S9032-02 are RGB color sensors using a 3-element photodiode with RGB sensitivity, assembled in one package.

Type No.	Spectral response range (nm)		Peak sensitivity wavelength (nm)	Active area (mm)		Dark current $V_R=1\text{ V}$ Max. (pA)	Package
S6428-01	400 to 540		460	2.4 × 2.8		20	① Plastic
S6429-01	480 to 600		540				
S6430-01	590 to 720		660				
S7505-01 NEW	Blue	400 to 540	460	Blue	1.5 × 1.5 (× 2)	200 *	② Surface mount plastic
	Green	480 to 600	540	Green	1.5 × 1.5		
	Red	590 to 720	620	Red	1.5 × 1.5		
S8751 NEW	Blue	400 to 540	460	1 × 1		100 *	③ Surface mount plastic
	Green	480 to 600	540				
	Red	590 to 720	660				
S8752 NEW	Blue	400 to 540	460	1 × 1		100 *	④ Plastic
	Red	590 to 720	660				
S9032-02 NEW	Blue	400 to 540	460	φ2/3 elements		100 *	⑤ Surface mount plastic
	Green	480 to 600	540				
	Red	590 to 720	620				
S8753 NEW	Photodiode a	320 to 1000	720	1.3 × 1.3		100	⑥ Plastic
	Photodiode b	800 to 1100	960				

* All elements in total



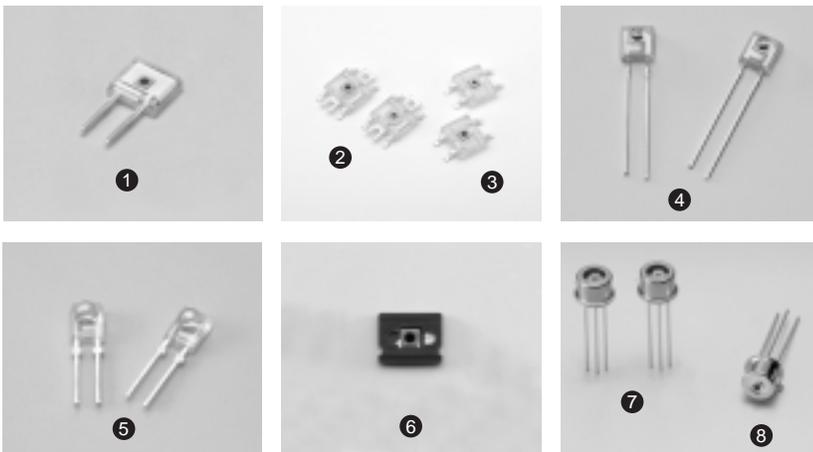
Si PIN photodiode

Si PIN photodiodes deliver high-speed response when operated with a reverse bias and are widely used for optical communications and optical disk pickup.

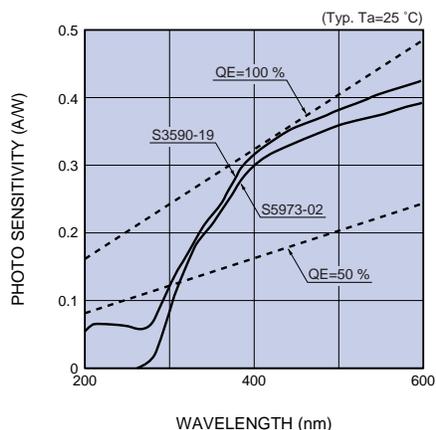
Cut-off frequency: 500 MHz or more

These Si PIN photodiodes deliver a wide bandwidth even with a low bias, making them ideal for high-speed photometry as well as optical communications. When connected to a high-speed preamplifier, their low terminal capacitance ensures a wide bandwidth because the input capacitance can be made smaller. Various types are provided, including those with mini lens that increases fiber-coupling efficiency and with enhanced violet sensitivity applicable to violet laser detection.

Type No.	Cut-off frequency (MHz)	Active area (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Package	Remark		
S8314	500 (VR=5 V)	φ0.8	320 to 1000	800	Plastic			
S7762	500 (VR=2.5 V)			φ0.6		760	①	
S6431							②	With mounting terminal
S7481							③	
S8387							④	Violet sensitivity enhanced
S8348 NEW		600 (VR=2.5 V)					φ0.6	760
S7482	③							
S8701	550 (VR=2 V)	φ1.7 (lens diameter)		760		④		With φ1.7 mm lens
S5052	500 (VR=5 V)	φ3 (lens diameter)		800		⑤		With φ3 mm lens
S7797	500 (VR=2.5 V)			760				
S8910-01 NEW	500 (VR=2.5 V)	φ0.8	760	⑥	Surface mount, miniature ceramic	Violet sensitivity enhanced		
S5972	500 (VR=10 V)	φ0.8	800	⑦	TO-18			
S5973	1.2 GHz (VR=3.3 V)	φ0.4	760	⑦				
S5973-01				⑧		With mini lens		
S5973-02				⑦		Violet sensitivity enhanced		
S7911	2 GHz (VR=2 V)	φ0.1	740	⑦			Low capacitance: 0.45 pF (VR=2 V)	
S8591						Low capacitance: 0.3 pF (VR=2 V)		
S7912	1.5 GHz (VR=2 V)	φ0.2	740	⑦		Low capacitance: 0.85 pF (VR=2 V)		
S9055 NEW			700		Low capacitance: 0.8 pF (VR=2 V)			

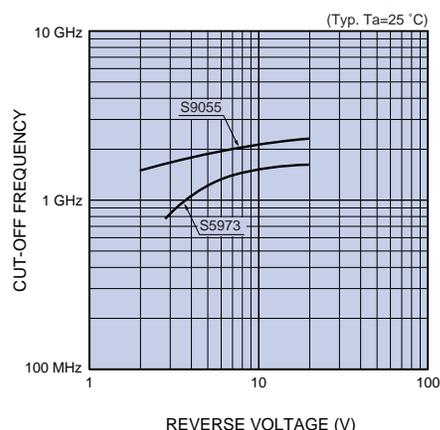


■ Spectral response (High violet sensitivity type: S5973-02, S3590-19: listed on page 9)



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■ Cut-off frequency vs. reverse voltage

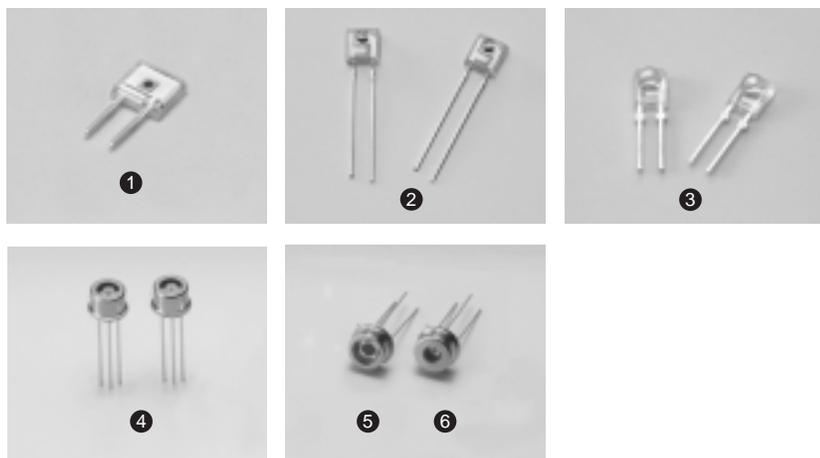


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Cut-off frequency: 100 MHz to less than 500 MHz

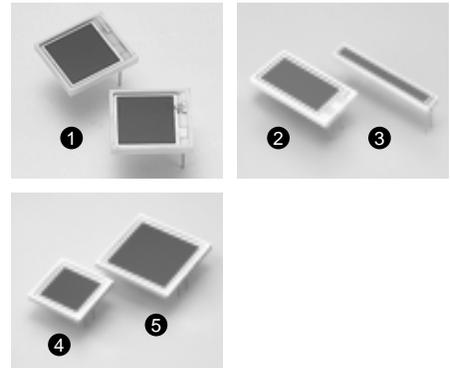
These Si PIN photodiodes have a large active area ($\phi 0.8$ to $\phi 3.0$ mm) yet deliver excellent frequency response characteristics (100 to 300 MHz), making them suitable for spatial light transmission and high-speed pulsed light detection.

Type No.	Cut-off frequency (MHz)	Active area (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Package
S8223	200 ($V_R=5$ V)	$\phi 0.8$	320 to 1060	900	① Plastic
S8359		$\phi 1.7$ (lens diameter)			② Plastic with $\phi 1.7$ mm lens
S8255		$\phi 3$ (lens diameter)			③ Plastic with $\phi 3$ mm lens
S5971	100 ($V_R=10$ V)	$\phi 1.2$	320 to 1000	840	④ TO-18
S3399		$\phi 3$			⑤ TO-5
S3883	300 ($V_R=20$ V)	$\phi 1.5$			⑥ TO-5



Large active area type

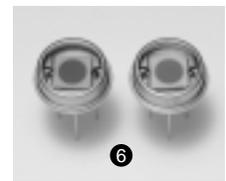
These Si PIN photodiodes, mounted on a white ceramic base, are developed specifically for applications in high energy physics. Because of high resistance to breakdown voltages, these Si PIN photodiodes operate at high reverse voltages allowing a high-speed response despite the large active areas. When coupled to BGO or CsI scintillators, these photodiodes can be used as the detectors for high energy particles. To improve photodiode-to-scintillator coupling efficiency, we also offer photodiodes with epoxy coating windows processed to have a flat surface (flatness: $\pm 5 \mu\text{m}$)



Type No.	Cut-off frequency (MHz)	Terminal capacitance $f=1 \text{ MHz}$ (pF)	Active area (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Package	Remark	
S3590-01	35 ($V_R=30 \text{ V}$)	75 ($V_R=30 \text{ V}$)	10 × 10	320 to 1060	920	Ceramic		
S3590-05	20 ($V_R=100 \text{ V}$)	25 ($V_R=100 \text{ V}$)	9 × 9	320 to 1120	980			
S3590-08	40 ($V_R=70 \text{ V}$)	40 ($V_R=70 \text{ V}$)	10 × 10	320 to 1100	960		①	Violet sensitivity enhanced
S3590-18								Bare chip type
S3590-19								Violet sensitivity enhanced
S8650								Flat surface ideal for bonding to scintillator
S2744-08	25 ($V_R=70 \text{ V}$)	85 ($V_R=70 \text{ V}$)	10 × 20	320 to 1100	960		②	
S3204-05	20 ($V_R=100 \text{ V}$)	80 ($V_R=100 \text{ V}$)	18 × 18	320 to 1120	980		④	
S3204-08	20 ($V_R=70 \text{ V}$)	130 ($V_R=70 \text{ V}$)	18 × 18	320 to 1100	960			
S3584-05	10 ($V_R=100 \text{ V}$)	200 ($V_R=100 \text{ V}$)	28 × 28	320 to 1120	980		⑤	
S3584-08	10 ($V_R=70 \text{ V}$)	300 ($V_R=70 \text{ V}$)	28 × 28	320 to 1100	960			
S3588-08	40 ($V_R=70 \text{ V}$)	40 ($V_R=70 \text{ V}$)	3 × 30	320 to 1100	960		③	

For YAG laser detection

S3759 is a Si PIN photodiode developed to detect and measure infrared energy emitted from YAG lasers ($1.06 \mu\text{m}$). Compared to standard Si photodiodes, S3759 delivers exceptionally high sensitivity of 0.38 A/W at $1.06 \mu\text{m}$. The PIN structure allows high-speed response and low capacitance. The active area is as large as $\phi 5 \text{ mm}$, making optical axis alignment easier.



Type No.	Active area (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Dark current $V_R = 100 \text{ V}$ Max. (nA)	Package
S3759	$\phi 0.5$	360 to 1120	980	10	⑥ TO-8

Si photodiode array

Si photodiode arrays consist of multiple elements of the same size, formed in a linear or matrix arrangement at an equal spacing in one package. These Si photodiode arrays are used in a wide range of applications such as laser beam position detection and spectrophotometry.

UV to near IR range: UV sensitivity enhanced type

These are Si photodiode linear arrays having rectangular elements equally spaced at a pitch of about 1 mm. Spectral response covers a wide range from UV to near IR, making these linear arrays suitable for low-light-level detection such as spectrophotometry. The cross-talk between elements is low so that the signal purity is maintained.

(Per 1 element)

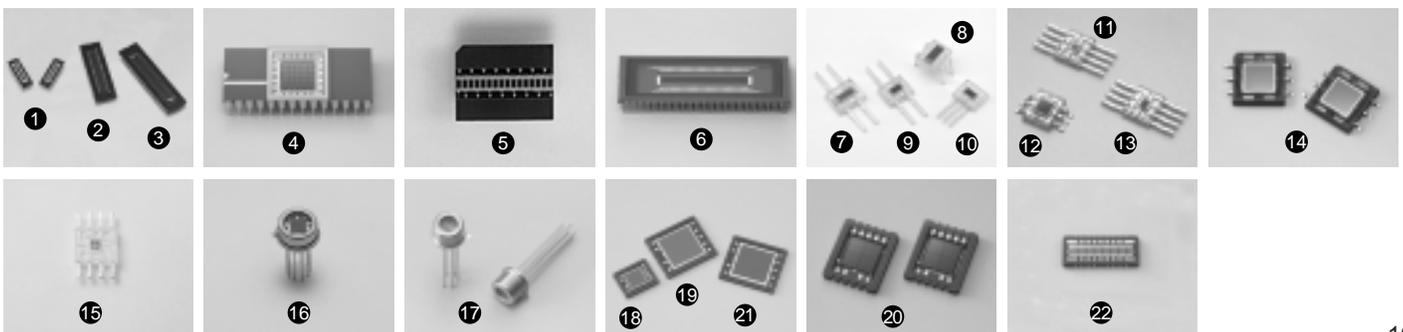
Type No.	Number of element	Active area (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Dark current VR = 10 mV Max. (pA)	Package	Remark
S4111-16Q	16	1.45 × 0.9	190 to 1100	960	5	①	Enhanced infrared sensitivity, low dark current
S4111-16R			320 to 1100				
S4111-35Q	35	4.4 × 0.9	190 to 1100	960	10	②	
S4111-46Q	46					③	
S4114-35Q	35		190 to 1000	800	60	②	
S4114-46Q	46					③	
S8592	16	1.45 × 0.9	320 to 1000	720	20	①	
S8593	5 × 5	1.3 × 1.3				④	
S5668-01	16	1.175 × 2.0	320 to 1100	960	1	⑤	Low dark current
S5668-02					5		
S3954	76	0.318 × 3.175	190 to 1100	960	30	⑥	Ceramic Element pitch: 0.3425 mm

Si PIN photodiode array (1)

These Si PIN photodiode arrays consist of 2 or 4 elements having sensitivity in the UV to near IR range. Since the active areas are formed in one or two dimensions, these photodiode arrays are used for position detection and laser beam alignment. A surface mount type ideal for automated production applications and a violet sensitivity enhanced type for violet laser detection are also available.

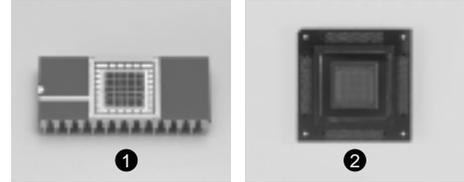
Type No.	Number of element	Active area (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Cut-off frequency (MHz)	Package
S2721-02	2	1 × 3	320 to 1060	900	50 (VR= 10 V)	⑦
S3096-02		1.2 × 3			25 (VR= 10 V)	⑧
S4204		1 × 2	320 to 1100	960	30 (VR= 10 V)	⑨
S8703						⑩
S7379-01	4	φ1	320 to 1060	900	80 (VR= 10 V)	⑪
S6695-01		2 × 2			40 (VR= 5 V)	⑫
S6058		0.6 × 1.2	320 to 1000	800	150 (VR= 3 V)	⑬
S7479		5 × 5	320 to 1100	960	20 (VR= 10 V)	⑭
S6795	6 *1	0.15 × 0.15 (0.2 × 0.25)	320 to 1000	800	400 (VR= 5 V)	⑮
S4349	4	3 × 3	190 to 1000	720	20 (VR=5 V)	⑯
S8284		0.6 × 1.2				⑰
S5980		5 × 5	320 to 1100	960	25 (VR= 10 V)	⑱
S5981		10 × 10			20 (VR= 10 V)	⑲
S8594	2 × 2	2.475 × 2.475	320 to 1100	960	25 (VR= 10 V)	⑳
S5870	2	10 × 10			10 (VR= 10 V)	㉑
S8558	16	0.7 × 2			25 (VR= 10 V)	㉒

*1: (0.15 × 0.15)/quadrant + (0.2 × 0.25) × 2 elements



Si PIN photodiode array (2)

These Si PIN photodiode arrays consist of multiple elements formed in a matrix pattern. Each element measures 1.3×1.3 mm and is spaced at a pitch of 1.5 mm. The output from each element can be read out in parallel or randomly, thus allowing high-speed 2D photometry.



(Per 1 element)

Type No.	Number of element	Active area (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Cut-off frequency $V_R = 5$ V (MHz)	Package
S7585	5 × 5	1.3 × 1.3	320 to 1000	800	170	① Ceramic
S3805	16 × 16	1.3 × 1.3			100	② Glass epoxy

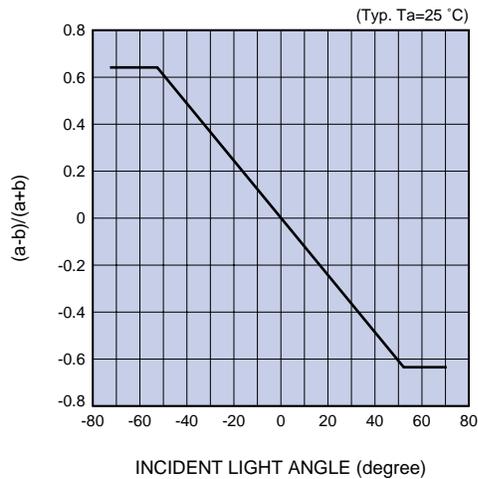
Incident light angle sensor

This sensor is designed to detect the incident light angle by processing the output current of 2-element Si PIN photodiode without using any lenses.



Type No.	Number of element	Active area (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Cut-off frequency $V_R = 10$ V (MHz)	Package
S6560	2	1.2 × 3.0	760 to 1100	960	25	Plastic

Example of angle detection characteristic (S6560)



$$\text{ANGLE} = \frac{a-b}{a+b} = 0.012 \text{ } ^\circ\text{-}^1$$

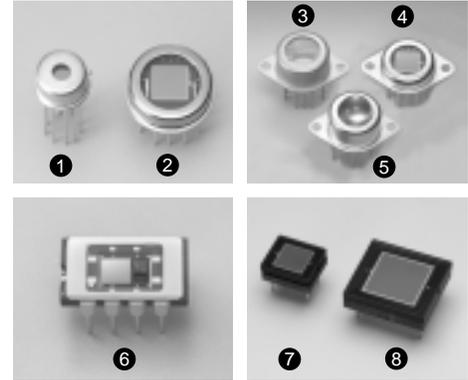
KPINB0213EA

Si photodiode with preamp, TE-cooled type Si photodiode

These Si photodiodes incorporate a photodiode and a preamplifier chip into the same package. This configuration makes them highly resistant to external noise and allows designing a compact circuit.

Si photodiode with preamp

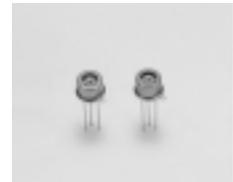
These are low noise photosensors incorporating a large area Si photodiode, operational amplifier and feedback capacitance. Suitable for a wide range of applications involving low-light-level detection such as analytical instrument and precision measurement. The active area of the photodiode is internally connected to the GND terminal making it highly resistant to EMC noise. TE-cooled types for use in NO_x detection are also available.



Type No.	Cooling temperature ΔT (°C)	Active area (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Package
S8745-01 NEW	Non-cooled	2.4 × 2.4	190 to 1100	960	Metal
S8746-01 NEW		5.8 × 5.8			
S9295 NEW	50	10 × 10	190 to 1100	960	
S9295-01 NEW	30				
S8785-02	50	φ15.6 (lens diameter)	320 to 1100		Metal with lens
S7998	Non-cooled	3 × 3	190 to 1100	880	Ceramic
S9269 NEW		5.8 × 5.8	320 to 1100	960	
S9270 NEW		10 × 10			

Si PIN photodiode with preamp for optical fiber communication

These high-speed photosensors consist of a Si PIN photodiode and a preamplifier chip integrated in the same package. These sensors deliver high-speed response and high sensitivity over a wide spectral range from the visible to near IR range. The small package (TO-18) allows a compact optical design. A violet sensitivity enhanced type for violet laser detection is also available.



Type No.	Cut-off frequency (MHz)	Active area (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Package
S6468	15	φ0.8	320 to 1060	900	TO-18
S6468-02	35		320 to 1000	800	

Si PIN photodiode with preamp for spatial light transmission

These sensors incorporate a Si PIN photodiode and a wide band (200 MHz) preamplifier. The photodiode has a relatively large active area ($\phi 3$ mm) yet offers a wide bandwidth, making these sensors suitable for spatial light transmission.



Type No.	Cut-off frequency (MHz)	Active area (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Package
S7516	170 *	$\phi 3$	320 to 1060	840	① TO-8
S7516-01		$\phi 9$ (lens diameter)			② TO-8 with lens

* 200 MHz at $R_L=500 \Omega$.

TE-cooled type Si photodiode

S2592/S3477 series sensors combine a UV to near infrared Si photodiode with a thermoelectric cooler. A thermistor is also included in the same package to sense the Si photodiode chip temperature. This allows stable operation over long periods of time, making these sensors suitable for low-light-level detection where a high S/N is required.

S2592 series is hermetically sealed in a TO-8 package, and S3477 series in a TO-66 package. A dedicated temperature controller (C1103-04) and heatsink (A3179 series) are also available as options (sold separately).



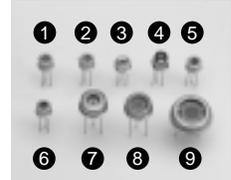
Type No.	Cooling temperature ΔT ($^{\circ}\text{C}$)	Active area (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Package
S2592-03	35	2.4×2.4	190 to 1100	960	③ TO-8
S2592-04		5.8×5.8			
S3477-03		2.4×2.4			④ TO-66
S3477-04		5.8×5.8			

Si APD (avalanche photodiode)

Si APDs are high-speed, high sensitivity photodiodes having an internal gain mechanism, and can be used in measurements at very low light levels.

Low bias operation type

These near infrared APDs are designed to be operated at low voltages. High gain can be obtained with voltages below 200 V, making these APDs suitable for spatial light transmission, rangefinder and optical fiber communications.

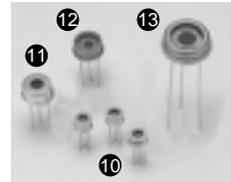


Type No.	Active area size (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Breakdown voltage (V)		Cut-off frequency (MHz)	Temp. coefficient of breakdown voltage (V/°C)	Gain	Package	
				Typ.	Max.					
S2381	φ0.2	400 to 1000	800	150	200	1000	0.65	100	①	TO-18
S2382	φ0.5					900			②	
S5139						③			TO-18 with lens	
S8611						④				
S2383	φ1.0					600			⑤	TO-18
S2383-10 *						⑥				
S3884	φ1.5					400			⑦	TO-5
S2384	φ3.0					120			⑧	TO-5
S2385	φ5.0					40			⑨	TO-8

* Variant type of S2383, with light-shield provided on the periphery of the element

Low temperature coefficient type

S6045 series is near infrared APDs designed to decrease the temperature coefficient of the breakdown voltage. Stable gain can be obtained over a wide temperature range, making these APDs suitable for spatial light transmission, rangefinder and optical fiber communications, etc.



Type No.	Active area size (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Breakdown voltage (V)		Cut-off frequency (MHz)	Temp. coefficient of breakdown voltage (V/°C)	Gain	Package	
				Typ.	Max.					
S6045-01	φ0.2	400 to 1000	800	200	300	1000	0.4	100	⑩	TO-18
S6045-02	φ0.5					900			⑪	
S6045-03	φ1.0					600			TO-5	
S6045-04	φ1.5					350				
S6045-05	φ3.0					80			⑫	
S6045-06	φ5.0					35			⑬	TO-8

Multi-element type

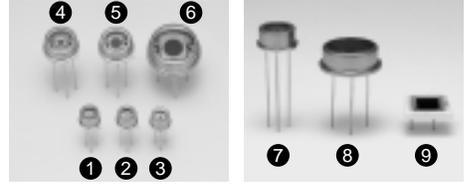
This quadrant APD with φ1 mm active area is designed to operate with a low bias. The quadrant format on one chip ensures uniform characteristics between elements. Single power supply operation allows easy connections. Applications include low-light-level detection and laser beam alignment.



Type No.	Active area size (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Breakdown voltage (V)		Cut-off frequency (MHz)	Temp. coefficient of breakdown voltage (V/°C)	Gain	Package
				Typ.	Max.				
S4402	φ1.0/4 elements	400 to 1000	800	150	200	310	0.65	100	TO-5

Short wavelength type

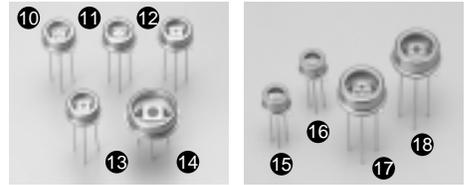
These short-wavelength APDs are optimized for detection of UV to visible light. High gain can be obtained in short wavelength regions, making these APDs suitable for low-light-level measurements such as in analytical instrument.



Type No.	Active area size (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Breakdown voltage (V)		Cut-off frequency (MHz)	Temp. coefficient of breakdown voltage (V/°C)	Gain	Package	
				Typ.	Max.				1	2
S9073 NEW	φ0.2	200 to 1000	620	150	200	900	0.14	50	1	TO-18
S9074 NEW	φ0.5								2	
S5343	φ1.0								3	
S9075 NEW	φ1.5								4	
S5344	φ3.0								5	
S5345	φ5.0								6	
S8664-02K NEW	φ0.2	320 to 1000	600	400	500	700	0.78	50	7	TO-5
S8664-05K NEW	φ0.5								8	
S8664-10K NEW	φ1.0								9	
S8664-20K NEW	φ2.0								TO-8	
S8664-30K NEW	φ3.0								TO-8	
S8664-50K NEW	φ5.0								TO-8	
S8664-55	5 x 5					40			9	Ceramic

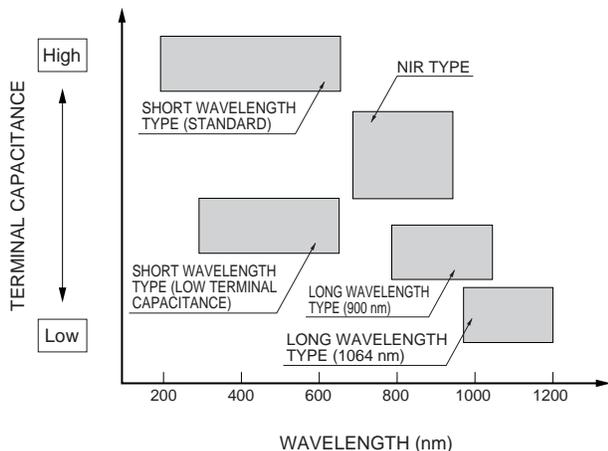
Long wavelength type

These long-wavelength APDs are optimized for detection of near infrared. High gain can be obtained in long wavelength regions, making these APDs suitable for YAG laser detection and rangefinder, etc.

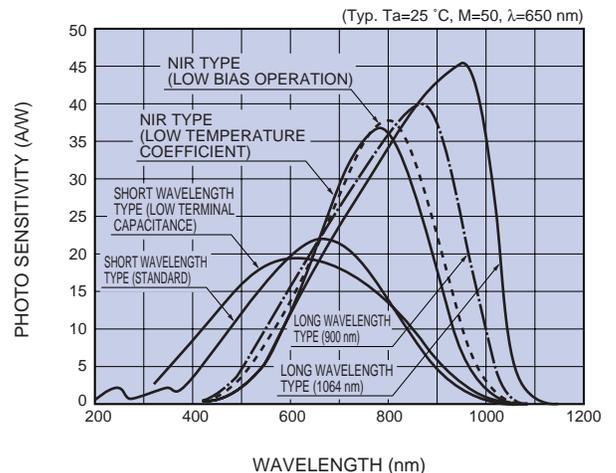


Type No.	Active area size (mm)	Spectral response range (nm)	Peak sensitivity wavelength (nm)	Breakdown voltage (V)		Cut-off frequency (MHz)	Temp. coefficient of breakdown voltage (V/°C)	Gain	Package	
				Typ.	Max.				10	11
S8890-02	φ0.2	400 to 1100	940	500	800	280	2.5	100	10	TO-5
S8890-05	φ0.5								11	
S8890-10	φ1.0								12	
S8890-15	φ1.5								13	
S8890-30	φ3.0								14	
S9251-02 NEW	φ0.2	440 to 1100	860	250	350	400	1.85	100	15	TO-18
S9251-05 NEW	φ0.5								16	
S9251-10 NEW	φ1.0								17	
S9251-15 NEW	φ1.5								18	
									TO-5	

Terminal capacitance vs. wavelength



Spectral response

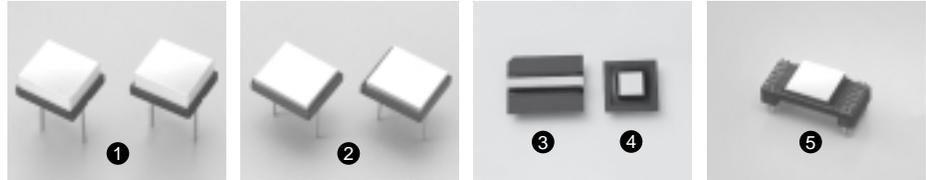


X-ray detector

These X-ray detectors are comprised of a Si photodiode coupled to a scintillator (ceramic or CsI). Ceramic scintillators have sensitivity to X-rays about 1.8 times higher than CWO and offer high reliability. CsI scintillators also have high sensitivity and are less expensive, but care is required when handling them at high humidity due to hygroscopic.

CsI scintillators used these detectors are suitable for X-ray tubes operated at 120 kV or less, and ceramic scintillators are optimized for X-ray tubes operated at 120 kV.

If detecting X-ray energy over 100 keV, it is necessary to redesign the scintillators. Please contact our sales office.

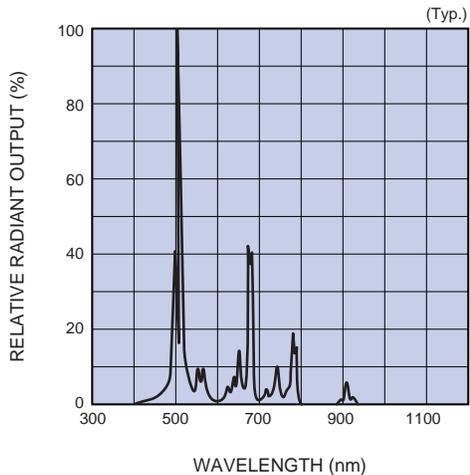


(Per 1 element)

Type No.	Scintillator	Active area (mm)	Number of element	Dark current Max. (pA)	X-ray sensitivity * (nA)	Package
S8559	CsI (Tl)	5.8 × 5.8	1	50	52	Ceramic
S8193	Ceramic				30	
S5668-11	CsI (Tl)	1.175 × 2.0/ch	16	10	5.8	Glass epoxy
S5668-34	Ceramic				3.1	
S7878		1.3 × 1.3/ch	1.2			
S7978		1.28 × 1.28/ch	2.1			

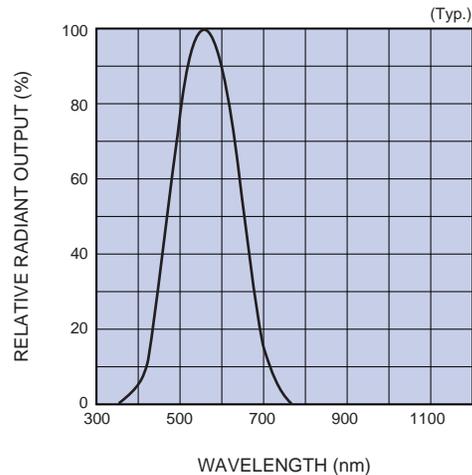
* These are for reference. [X-ray sensitivity depends on the X-ray equipment operating and setup conditions. (Measurement condition: X-ray tube voltage 120 kV, tube current 1.0 mA, aluminum filter t=6 mm, distance=830 mm)]

■ Emission spectrum of ceramic scintillator



KSPDB0189EA

■ Emission spectrum of CsI (Tl)



KSPDB0204EA

■ Typical scintillator characteristics

Parameter	Condition	CsI (Tl)	Ceramic scintillator	CWO	Unit
Peak emission wavelength		560	520	540	nm
X-ray absorption coefficient	100 keV	10	7	7.7	-
Refractive index	at peak emission wavelength	1.74	2.2	2.2	-
Decay constant		1	3	5	μs
Afterglow	100 ms after X-ray turn off	0.3	0.01	0.02	%
Density		4.51	7.34	7.9	g/cm ³
Relative emission intensity	CWO=1.0	1.8	1.8	1.0	-
Color		Transparent	Light yellow-green	Transparent	-
Sensitivity non-uniformity		±10	±5	±15	%

Description of terms

1. Spectral response

The photocurrent produced by a given level of incident light varies with the wavelength. This relation between the photoelectric sensitivity and wavelength is referred to as the spectral response characteristic and is expressed in terms of photo sensitivity, quantum efficiency, etc.

2. Photo sensitivity: S

This measure of sensitivity is the ratio of radiant energy expressed in watts (W) incident on the device, to the resulting photocurrent expressed in amperes (A). It may be represented as either an absolute sensitivity (A/W) or as a relative sensitivity normalized for the sensitivity at the peak wavelength, usually expressed in percent (%) with respect to the peak value. For the purpose of data sheet, the photo sensitivity is represented as the absolute sensitivity, and the spectral response range is defined as the region in which the relative sensitivity is higher than 5 % of the peak value.

3. Quantum efficiency: QE

The quantum efficiency is the number of electrons or holes that can be detected as a photocurrent divided by the number of the incident photons. This is commonly expressed in percent (%). The quantum efficiency and photo sensitivity S have the following relationship at a given wavelength (nm):

$$QE = \frac{S \times 1240}{\lambda} \times 100 [\%] \dots\dots\dots (1)$$

where S is the photo sensitivity in A/W at a given wavelength and λ is the wavelength in nm (nanometers).

4. Short circuit current: I_{sc}, open circuit voltage: Voc

The short circuit current is the output current which flows when the load resistance is 0 and is nearly proportional to the device active area. This is often called "white light sensitivity" with regards to the spectral response. This value is measured with light from a tungsten lamp of 2856 K distribution temperature (color temperature), providing 100 time illuminance. The open circuit voltage is a photovoltaic voltage developed when the load resistance is infinite and exhibits a constant value independent of the device active area.

5. Infrared sensitivity ratio

This is the ratio of the output current I_R measured with a light flux (2856 K, 100 time) passing through an R-70 (t=2.5 mm) infrared filter to the short circuit current I_{sc} measured without the filter. It is commonly expressed in percent, as follows:

$$\text{Infrared sensitivity ratio} = \frac{I_R}{I_{sc}} \times 100 [\%] \dots\dots\dots (2)$$

6. Dark current: I_D, shunt resistance: R_{sh}

The dark current is a small current which flows when a reverse voltage is applied to a photodiode even in dark state. This is a major source of noise for applications in which a reverse voltage is applied to photodiodes (PIN photodiode, etc.). In contrast, for applications where no reverse voltage is applied, noise resulting from the shunt resistance becomes predominant. This shunt resistance is the voltage-to-current ratio in the vicinity of 0 V and defined as follows:

$$R_{sh} = \frac{10 [\text{mV}]}{I_D} [\Omega] \dots\dots\dots (3)$$

where I_D is the dark current at V_R=10 mV.

7. Terminal capacitance: C_t

An effective capacitor is formed at the PN junction of a photodiode. Its capacitance is termed the junction capacitance and is one of parameters that determine the response speed of the photodiode. And it probably causes a phenomenon of gain peaking in I-V conversion circuit using operational amplifier. In Hamamatsu, the terminal capacitance including this junction capacitance plus package stray capacitance is listed.

8. Rise time: tr

This is the measure of the time response of a photodiode to a stepped light input, and is defined as the time required for the output to change from 10 % to 90 % of the steady output level. The rise time depends on the incident light wavelength and load resistance. For the purpose of data sheets, it is measured with a light source of GaAsP LED (655 nm) or GaP LED (560 nm) and load resistance of 1 k Ω .

9. Cut-off frequency: fc

This is the measure used to evaluate the time response of high-speed APD (avalanche photodiodes) and PIN photodiodes to a sinewave-modulated light input. It is defined as the frequency at which the photodiode output decreases by 3 dB from the output at 100 kHz. The light source used is a laser diode (830 nm) and the load resistance is 50 Ω . The rise time tr has a relation with the cut-off frequency fc as follows:

$$tr = \frac{0.35}{fc} \dots\dots\dots (4)$$

10. NEP (Noise Equivalent Power)

The NEP is the amount of light equivalent to the noise level of a device. Stated differently, it is the light level required to obtain a signal-to-noise ratio of unity. In data sheets lists the NEP values at the peak wavelength λ_p . Since the noise level is proportional to the square root of the frequency bandwidth, the NEP is measured at a bandwidth of 1 Hz.

$$NEP [W/Hz^{1/2}] = \frac{\text{Noise current [A/Hz}^{1/2}]}{\text{Photo sensitivity at } \lambda_p [A/W]} \dots\dots\dots (5)$$

11. Maximum reverse voltage: V_R Max.

Applying a reverse voltage to a photodiode triggers a breakdown at a certain voltage and causes severe deterioration of the device performance. Therefore the absolute maximum rating is specified for reverse voltage at the voltage somewhat lower than this breakdown voltage. The reverse voltage shall not exceed the maximum rating, even instantaneously.

Reference

● Physical constant

Constant	Symbol	Value	Unit
Electron charge	e or q	1.602 × 10 ⁻¹⁹	c
Speed of light in vacuum	c	2.998 × 10 ⁸	m/s
Planck's constant	h	6.626 × 10 ⁻³⁴	Js
Boltzmann's constant	k	1.381 × 10 ⁻²³	J/K
Room temperature thermal energy	KT (T=300 K)	0.0259	eV
1 eV energy	eV	1.602 × 10 ⁻¹⁹	J
Wavelength in vacuum corresponding to 1 eV	-	1240	nm
Dielectric constant of vacuum	ϵ_0	8.854 × 10 ⁻¹²	F/m
Dielectric constant of silicon	ϵ_{si}	Approx. 12	-
Dielectric constant of silicon oxide	ϵ_{ox}	Approx. 4	-
Energy gap of silicon	E _g	Approx. 1.12 (T=25 °C)	eV

Characteristic and use

Introduction

Photodiodes are semiconductor light sensors that generate a current or voltage when the P-N junction in the semiconductor is illuminated by light. The term photodiode can be broadly defined to include even solar batteries, but it usually refers to sensors used to detect the intensity of light. Photodiodes can be classified by function and construction as follows:

Photodiode type

- 1) PN photodiode
- 2) PIN photodiode
- 3) Schottky type photodiode
- 4) APD (Avalanche photodiode)

All of these types provide the following features and are widely used for the detection of the intensity, position, color and presence of light.

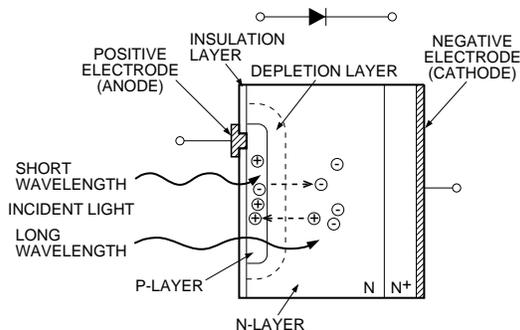
Features of photodiode

- 1) Excellent linearity with respect to incident light
- 2) Low noise
- 3) Wide spectral response
- 4) Mechanically rugged
- 5) Compact and lightweight
- 6) Long life

1. Principle of operation

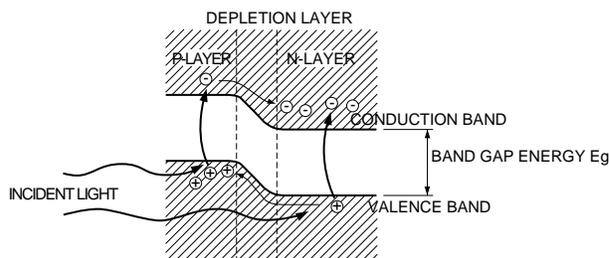
Figure 1-1 shows a cross section of a photodiode. The P-layer material at the active surface and the N material at the substrate form a PN junction which operates as a photoelectric converter. The usual P-layer for a Si photodiode is formed by selective diffusion of boron, to a thickness of approximately $1\ \mu\text{m}$ or less and the neutral region at the junction between the P- and N-layers is known as the depletion layer. By controlling the thickness of the outer P-layer, substrate N-layer and bottom N^+ -layer as well as the doping concentration, the spectral response and frequency response can be controlled. When light strikes a photodiode, the electron within the crystal structure becomes stimulated. If the light energy is greater than the band gap energy E_g , the electrons are pulled up into the conduction band, leaving holes in their place in the valence band. (See Figure 1-2) These electron-hole pairs occur throughout the P-layer, depletion layer and N-layer materials. In the depletion layer the electric field accelerates these electrons toward the N-layer and the holes toward the P-layer. Of the electron-hole pairs generated in the N-layer, the electrons, along with electrons that have arrived from the P-layer, are left in the N-layer conduction band. The holes at this time are being diffused through the N-layer up to the depletion layer while being accelerated, and collected in the P-layer valence band. In this manner, electron-hole pairs which are generated in proportion to the amount of incident light are collected in the N- and P-layers. This results in a positive charge in the P-layer and a negative charge in the N-layer. When an external circuit is connected between the electrodes formed on the P-layer and N-layer, electrons will flow away from the N-layer, and holes will flow away from the P-layer toward the opposite respective electrodes. These electrons and holes generating a current flow in a semiconductor are called the carriers.

Figure 1-1 Photodiode cross section



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Figure 1-2 Photodiode P-N junction state



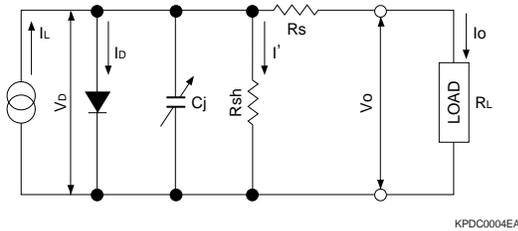
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2. Si photodiode

2-1. Equivalent circuit

An equivalent circuit of a photodiode is shown in Figure 2-1.

Figure 2-1 Photodiode equivalent circuit



- IL : Current generated by the incident light (proportional to the amount of light)
- ID : Diode current
- Cj : Junction capacitance
- Rsh : Shunt resistance
- Rs : Series resistance
- I' : Shunt resistance current
- VD : Voltage across the diode
- Io : Output current
- Vo : Output voltage

Using the above equivalent circuit, the output current Io is given as follows:

$$I_o = I_L - I_D - I' = I_L - I_s \left(\exp \frac{eV_D}{kT} - 1 \right) - I' \dots\dots\dots (2-1)$$

- Is : Photodiode reverse saturation current
- e : Electron charge
- k : Boltzmann's constant
- T : Absolute temperature of the photodiode

The open circuit voltage Voc is the output voltage when Io equals 0. Thus Voc becomes

$$V_{oc} = \frac{kT}{e} \ln \left(\frac{I_L - I'}{I_s} + 1 \right) \dots\dots\dots (2-2)$$

If I' is negligible, since Is increases exponentially with respect to ambient temperature, Voc is inversely proportional to the ambient temperature and proportional to the log of IL. However, this relationship does not hold for very low light levels.

The short circuit current Isc is the output current when the load resistance RL equals 0 and Vo equals 0, yielding:

$$I_{sc} = I_L - I_s \left(\exp \frac{e \cdot (I_{sc} \cdot R_s)}{kT} - 1 \right) - \frac{I_{sc} \cdot R_s}{R_{sh}} \dots\dots (2-3)$$

In the above relationship, the 2nd and 3rd terms limit the linearity of Isc. However, since Rs is several ohms and Rsh is 10⁷ to 10¹¹ ohms, these terms become negligible over quite a wide range.

2-2. Current vs. voltage characteristic

When a voltage is applied to a photodiode in the dark state, the current vs. voltage characteristic observed is similar to the curve of a conventional rectifier diode as shown in Figure 2-2 ①. However, when light strikes the photodiode, the curve at ① shifts to ② and, increasing the amount of incident light shifts this characteristic curve still further to position ③ in parallel, according to the incident light intensity. As for the characteristics of ② and ③, if the photodiode terminals are shorted, a photocurrent Isc or Isc proportional to the light intensity will flow in the direction from the anode to the cathode. If the circuit is open, an open circuit voltage Voc or Voc' will be generated with the positive polarity at the anode. The short circuit current Isc is extremely linear with respect to the incident light level. When the incident light is within a range of 10⁻¹² to 10⁻² W, the achievable range of linearity is higher than 9 orders of magnitude, depending on the type of photodiode and its operating circuit. The lower limit of this linearity is determined by the NEP, while the upper limit depends on the load resistance and reverse bias voltage, and is given by the following equation:

$$P_{sat} = \frac{V_{Bi} + V_R}{(R_s + R_L) \cdot S_\lambda} \dots\dots\dots (2-4)$$

- Psat : Input energy (W) at upper limit of linearity Psat ≤ 10 mW
- VBi : Contact voltage (V) <0.2 to 0.3 V>
- VR : Reverse voltage (V)
- RL : Load resistance (Ω)
- Sλ : Photo sensitivity at wavelength λ (A/W)
- Rs : Photodiode series resistance (several Ω)

When laser light is condensed on a small spot, however, the actual series resistance element increases, and linearity deteriorates.

Voc varies logarithmically with respect to a change of the light level and is greatly affected by variations in temperature, making it unsuitable for light intensity measurements. Figure 2-3 shows the result of plotting Isc and Voc as a function of incident light illuminance.

Figure 2-2 Current vs. voltage characteristic

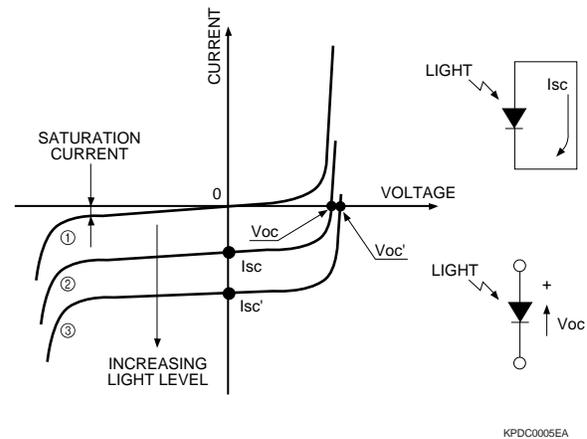
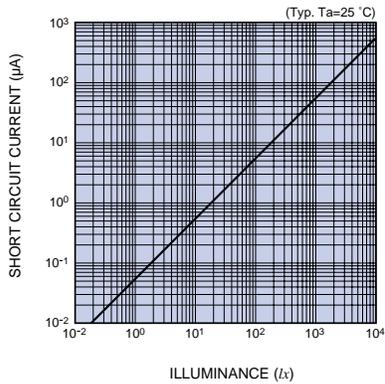


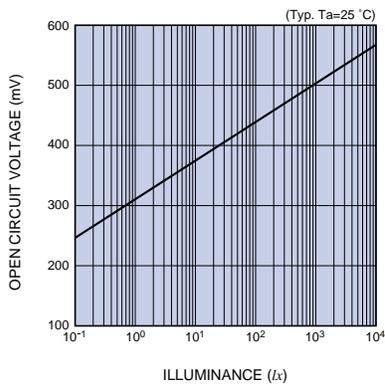
Figure 2-3 Output signal vs. incident light level (S2386-5K)

(a) Short circuit current



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(b) Open circuit voltage

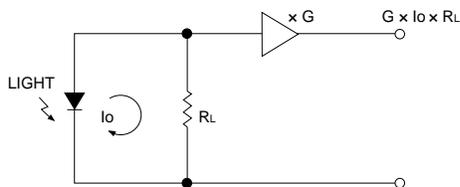


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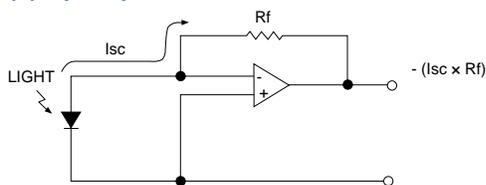
Figure 2-4 (a) and (b) show methods of measuring light by measuring the photocurrent I_L or I_{sc} . In the circuit shown at (a), the voltage ($I_o \times R_L$) is amplified by an amplifier with gain G , although the circuit does have limitations on its linearity according to equation (2-4). This condition is shown in Figure 2-5. Figure 2-4 (b) is a circuit using an operational amplifier. If we set the open loop gain of the operational amplifier as A , the characteristics of the feedback circuit allows the equivalent input resistance (equivalent to load resistance R_L) to be $\frac{R_f}{A}$ which is several orders of magnitude smaller than R_f . Thus this circuit enables ideal I_{sc} measurement over a wide range. For measuring a wide range, R_L and R_f must be adjusted as needed.

Figure 2-4 Photodiode operational circuits

(a) Load resistance circuit

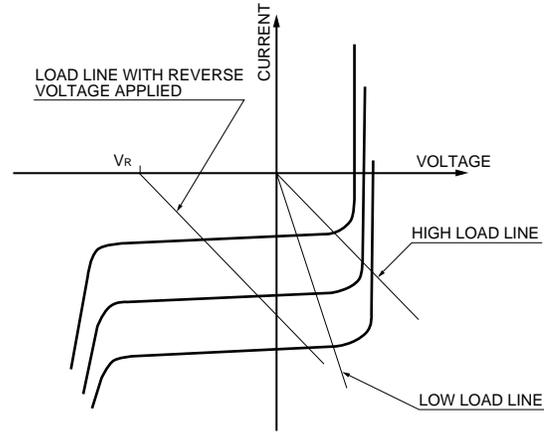


(b) Op-amp circuit



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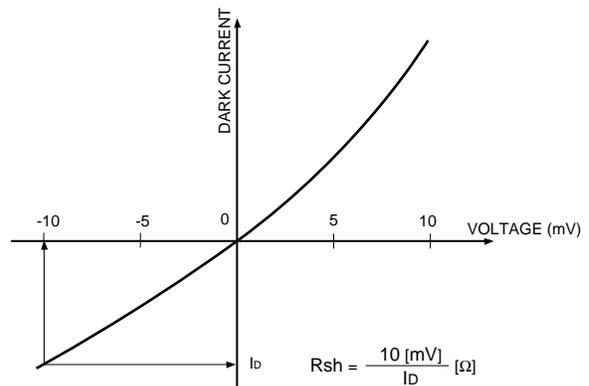
Figure 2-5 Current vs. voltage characteristic and load line



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If the zero region of Figure 2-2 ① is magnified, we see, as shown in Figure 2-6, that the dark current I_D is approximately linear in a voltage range of about ± 10 mV. The slope in this region indicates the shunt resistance R_{sh} and this resistance is the cause of the thermal noise current described later. In data sheets, values of R_{sh} are given using a dark current I_D measured with -10 mV applied.

Figure 2-6 Dark current vs. voltage (Enlarged zero region)



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2-3. Spectral response

As explained in the section on principle of operation, when the energy of absorbed light is lower than the band gap energy E_g , the photovoltaic effect does not occur. The limiting wavelength λ_h can be expressed in terms of E_g as follows:

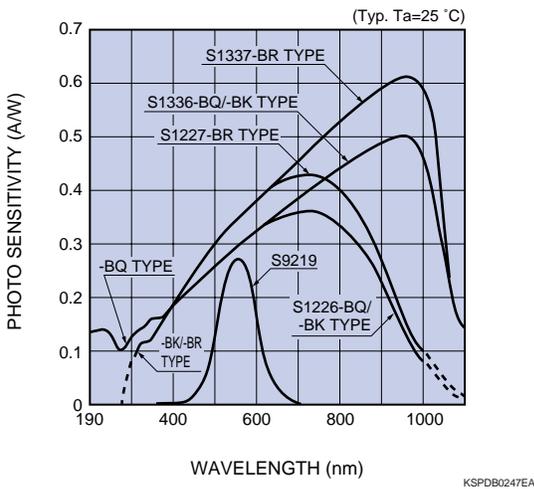
$$\lambda_h = \frac{1240}{E_g} \text{ [nm]} \dots\dots\dots (2-5)$$

At room temperatures, E_g is 1.12 eV for Si and 1.8 eV for GaAsP, so that the limiting wavelength will be 1100 nm and 700 nm, respectively. For short wavelengths, however, the degree of light absorption within the surface diffusion layer becomes very large. Therefore, the thinner the diffusion layer is and the closer the P-N junction is to the surface, the higher the sensitivity will be. (See Figure 1-1.) For normal photodiodes the cut-off wavelength is 320 nm, whereas for UV-enhanced photodiodes (e.g. S1226/S1336 series) it is 190 nm.

The cut-off wavelength is determined by the intrinsic material properties of the photodiode, but it is also affected by the spectral transmittance of the window material. For borosilicate glass and plastic resin coating, wavelengths below approximately 300 nm are absorbed. If these materials are used as the window, the short wavelength sensitivity will be lost. For wavelengths below 300 nm, photodiodes with quartz windows are used. For measurements limited to the visible light region, a visual-compensation filter is used as the light-receiving window.

Figure 2-7 shows the spectral response characteristics for various photodiode types. The BQ type shown uses a quartz window, the BK type a borosilicate glass window and the BR type a resin-coated window. S9219 is a visible photodiode with a visual-compensated filter.

Figure 2-7 Spectral response example



2-4. Noise characteristic

Like other types of light sensors, the lower limits of light detection for photodiodes are determined by the noise characteristics of the device. The photodiode noise is the sum of the thermal noise (or Johnson noise) *ij* of a resistor which approximates the shunt resistance and the shot noise *isD* and *isL* resulting from the dark current and the photocurrent.

$$in = \sqrt{ij^2 + isD^2 + isL^2} \text{ [A]} \dots\dots\dots (2-6)$$

ij is viewed as the thermal noise of Rsh and is given as follows:

$$ij = \sqrt{\frac{4kTB}{Rsh}} \text{ [A]} \dots\dots\dots (2-7)$$

k: Boltzmann's constant
 T: Absolute temperature of the element
 B: Noise bandwidth

When a bias voltage is applied as in Figure 3-1, there is always a dark current. The shot noise *isD* originating from the dark current is given by

$$isD = \sqrt{2qIdB} \text{ [A]} \dots\dots\dots (2-8)$$

q: Electron charge
 Id: Dark current
 B: Noise bandwidth

When IL (photocurrent) exists, *isL* is given by application of incident light, a photocurrent IL exists so *isL* is given by

$$isL = \sqrt{2qILB} \text{ [A]} \dots\dots\dots (2-9)$$

If $IL \gg 0.026/Rsh$ or $IL \gg Id$, the shot noise current of equation (2-9) becomes predominant instead of the noise factor of equation (2-7) or (2-8).

The amplitudes of these noise sources are each proportional to the square root of the measured bandwidth B so that they are expressed in units of A/Hz^{1/2}.

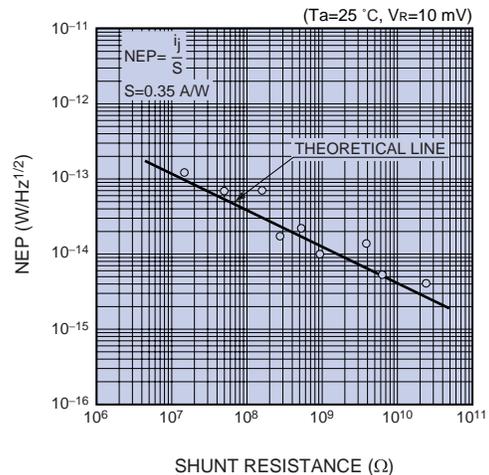
The lower limit of light detection for a photodiode is usually expressed as the intensity of incident light required to generate a current equal to the noise current as expressed in equation (2-7) or (2-8). Essentially this is the noise equivalent power (NEP).

$$NEP = \frac{in}{S} \text{ [W/Hz}^{1/2}] \dots\dots\dots (2-10)$$

in: Noise current (A/Hz^{1/2})
 S: Photo sensitivity (A/W)

In cases where *ij* is predominant, the relation between NEP and shunt resistance of a photodiode is plotted as shown in Figure 2-8. This relation agrees with the theoretical data.

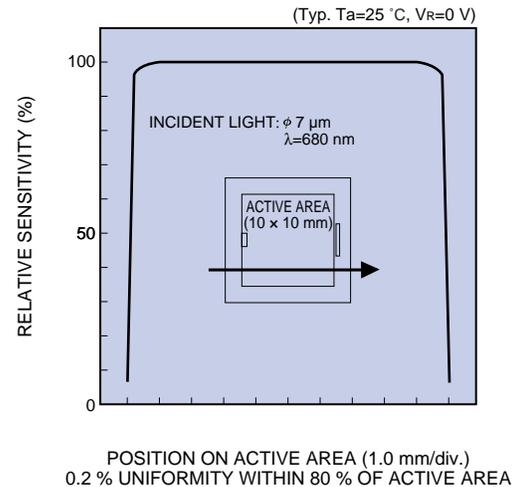
Figure 2-8 NEP vs. shunt resistance (S1226-5BK)



2-5. Spatial response uniformity

This is the measure of the variation in sensitivity with the position of the active area. Photodiodes offer excellent uniformity, usually less than 1 %. This uniformity is measured with light from a laser diode condensed to a small spot from several microns to several dozen microns in diameter.

Figure 2-9 Spatial response uniformity (S1227-1010BQ)

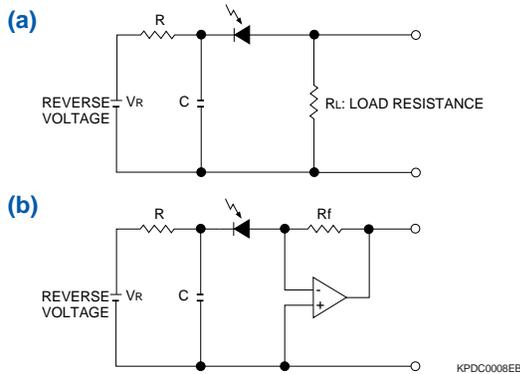


3. Si PIN photodiode

3-1. Reverse voltage

Because photodiodes generate a power due to the photovoltaic effect, they can operate without the need for an external power source. However, frequency response and linearity can be improved by using an external reverse voltage V_R . It should be borne in mind that the signal current flowing in a photodiode circuit is determined by the number of photovoltaically generated electron-hole pairs and that the application of a reverse voltage does not affect the signal current nor impair the photoelectric conversion linearity. Figure 3-1 shows examples of reverse voltage connection. Figures 3-2 and 3-3 show the effect of reverse voltage on cut-off frequency and linearity limits, respectively. While application of a reverse voltage to a photodiode is very useful in improving frequency response and linearity, it has the accompanying disadvantage of increasing dark current and noise levels along with the danger of damaging the device by excessive applied reverse voltage. Thus, care is required to maintain the reverse voltage within the maximum ratings and to ensure that the cathode is maintained at a positive potential with respect to the anode.

Figure 3-1 Reverse voltage connection



For use in applications such as optical communications and remote control which require high response speed, the PIN photodiode provides not only good response speed but excellent dark current and voltage resistance characteristics with reverse voltage applied. Note that the reverse voltages listed in data sheets are recommended values and each PIN photodiode is designed to provide optimum performance at the recommended reverse voltage.

Figure 3-2 Cut-off frequency vs. reverse voltage (S5973, S9055)

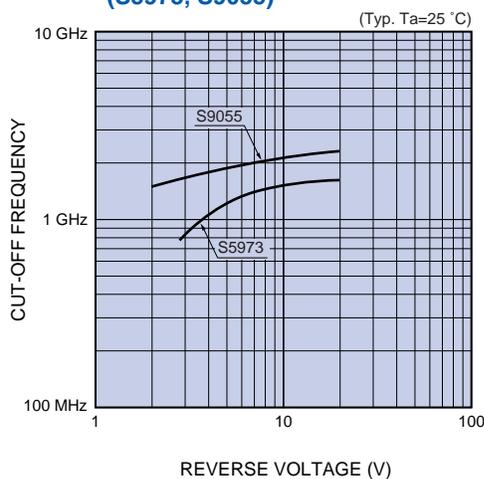


Figure 3-3 Output current vs. illuminance (S1223)

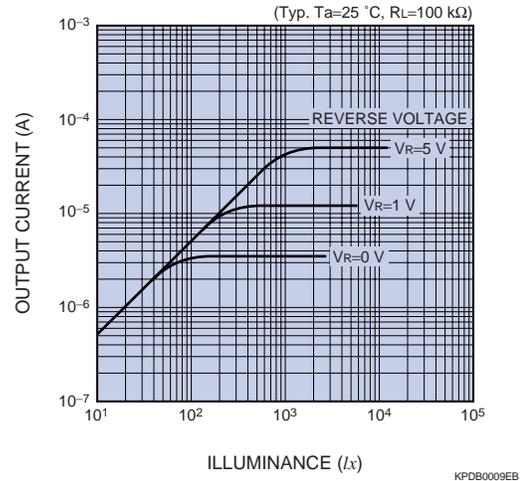
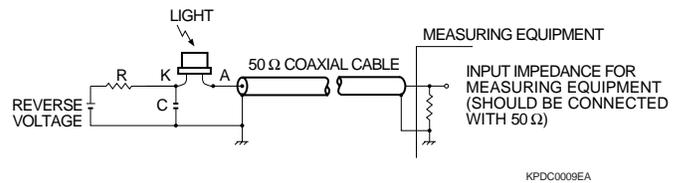


Figure 3-4 shows an example of the actual connection shown in Figure 3-1 (b) with a load resistance 50Ω . The ceramic capacitor C is used to enable a reduction of the bias supply impedance, while resistor R is used to protect the photodiode. The resistor value is selected such that the voltage drop caused by the maximum photocurrent is sufficiently smaller than the reverse voltage. The photodiode and capacitor leads, coaxial cable and other wire carrying high-speed pulses should be kept as short as possible.

Figure 3-4 Connection to coaxial cable



3-2. Response speed and frequency response

The response speed of a photodiode is a measure of the time required for the accumulated charge to become an external current and is generally expressed as the rise time or cut-off frequency. The rise time is the time required for the output signal to change from 10 % to 90 % of the peak output value and is determined by the following factors:

1) Terminal capacitance C_t and time constant t_1 of load resistance R_L

Time constant t_1 determined by the terminal capacitance C_t of the photodiode and the load resistance R_L . C_t is the sum of the package capacitance and the photodiode junction capacitance. t_1 is given by

$$t_1 = 2.2 \times C_t \times R_L \dots\dots\dots (3-1)$$

To shorten t_1 , the design must be such that C_t or R_L is made smaller. C_j is nearly proportional to the active area A and inversely proportional to the second to third root of the depletion layer width d . Since the depletion layer width is proportional to the product of the resistivity ρ of the substrate material and reverse voltage V_R , the following equation is established as:

$$C_j \propto A \{(V_R + 0.5) \times \rho\}^{-1/2 \text{ to } -1/3} \dots\dots\dots (3-2)$$

Accordingly, to shorten t_1 , a photodiode with a small A and large ρ should be used with a reverse voltage applied. However, reverse voltage also increases dark current so caution is necessary for use in low-light-level detection.

2) Diffusion time t_2 of carriers generated outside the depletion layer

Carriers may generate outside the depletion layer when incident light misses the P-N junction and is absorbed by the surrounding area of the photodiode chip and the substrate section which is below the depletion area. The time t_2 required for these carriers to diffuse may sometimes be greater than several microseconds.

3) Carrier transit time t_3 in the depletion layer

The transit speed v_d at which the carriers travel in the depletion layer is expressed using the traveling rate μ and the electric field E developed in the depletion layer, as in $v_d = \mu E$. If we let the depletion layer width be d and the applied voltage be V_R , the average electric field $E = V_R/d$, and thus t_3 can be approximated as follows:

$$t_3 = d / v_d = d^2 / (\mu V_R) \dots\dots\dots (3-3)$$

To achieve a fast response time for t_3 , the moving distance of carriers should be short and the reverse voltage larger.

The above three factors determine the rise time t_r of a photodiode and rise time t_r is approximated by the following equation:

$$t_r = \sqrt{t_1^2 + t_2^2 + t_3^2} \dots\dots\dots (3-4)$$

PIN photodiodes and avalanche photodiodes are designed such that less carriers are generated outside the depletion layer, C_t is small and the carrier transit time in the depletion layer is short. Therefore, these types are ideally suited for high-speed light detection.

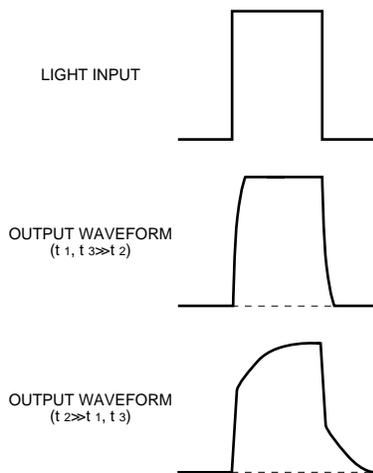
The cut-off frequency f_c is the frequency at which the photodiode output drops by 3 dB relative to the steady-state output at low frequency regions when the photodiode receives sinewave-modulated light emitted from a laser diode.

The rise time t_r is roughly approximated by the following relational expression:

$$t_r = \frac{0.35}{f_c} \dots\dots\dots (3-5)$$

Figures 3-5 (a), (b) and (c) show examples of the response waveform and frequency response characteristics for typical photodiodes.

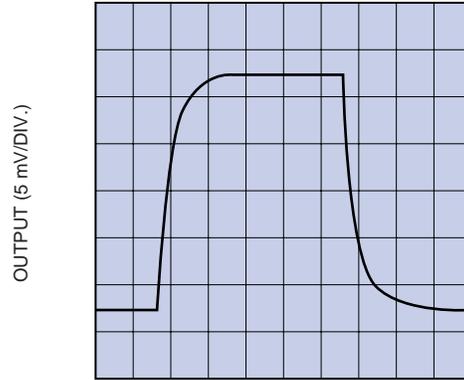
Figure 3-5 (a) Photodiode response waveform example



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(b) Response waveform (S2386-18K)

(Typ. $T_a=25^\circ\text{C}$, $\lambda=655\text{ nm}$, $V_R=0\text{ V}$, $R_L=1\text{ k}\Omega$)

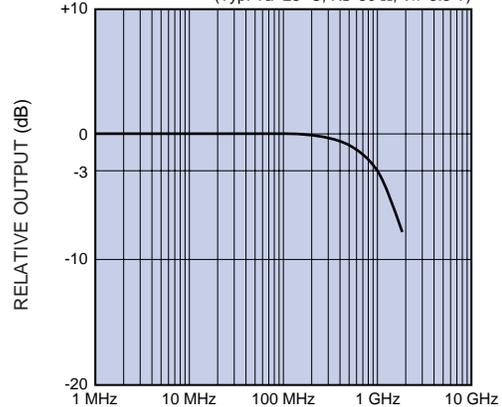


TIME (500 ns/DIV.)

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(c) Frequency response (S5973)

(Typ. $T_a=25^\circ\text{C}$, $R_L=50\ \Omega$, $V_R=3.3\text{ V}$)



FREQUENCY

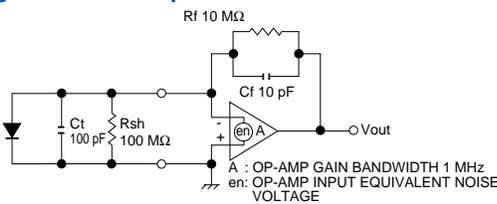
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4. Si photodiode with preamp

4-1. Feedback circuit

Figure 4-1 shows a basic circuit connection of an operational amplifier and photodiode. The output voltage V_{out} from DC through the low-frequency region is 180 degrees out of phase with the input current I_{sc} . The feedback resistance R_f is determined by I_{sc} and the required output voltage V_{out} . If, however, R_f is made greater than the photodiode internal resistance R_{sh} , the operational amplifier's input noise voltage e_n and offset voltage will be multiplied by $(1 + \frac{R_f}{R_{sh}})$. This is superimposed on the output voltage V_{out} , and the operational amplifier's bias current error (described later) will also increase. It is therefore not practical to use an infinitely large R_f . If there is an input capacitance C_t , the feedback capacitance C_f prevents high-frequency oscillations and also forms a lowpass filter with a time constant $C_f \times R_f$ value. The value of C_f should be chosen according to the application. If the input light is similar to a discharge spark, and it is desired to integrate the amount of light, R_f can be removed so that the operational amplifier and C_f act as an integrating circuit. However, a switch is required to discharge C_f before the next integration.

Figure 4-1 Basic photodiode connection



4-2. Bias current

Since the actual input impedance of an operational amplifier is not infinite, some bias current that will flow into or out of the input terminals. This may result in error, depending upon the magnitude of the detected current. The bias current which flows in an FET input operational amplifier is sometimes lower than 0.1 pA. Bipolar operational amplifiers, however, have bias currents ranging from several hundred pA to several hundred nA. However, the bias current of an FET operational amplifier increases two-fold for every increase of 5 to 10 °C in temperature, whereas that of bipolar amplifiers decreases with increasing temperature. The use of bipolar amplifiers should be considered when designing circuits for high temperature operation.

As is the case with offset voltage, the error voltage attributable to the bias current can be adjusted by means of a potentiometer connected to the offset adjustment terminals. Furthermore, leakage currents on the PC board used to house the circuit may be greater than the operational amplifier's bias current. Consideration must be given to the circuit pattern design and parts layout, as well as the use of Teflon terminals and guard rings.

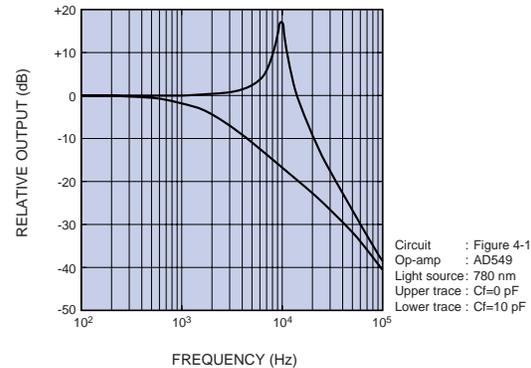
4-3. Gain peaking

The frequency response of a photodiode and operational amplifier circuit is determined by the time constant $R_f \times C_f$. However, for large values of terminal capacitance (i.e. input capacitance) a phenomenon known as gain peaking will occur. Figure 4-2 shows an example of such a frequency response. It can be seen from the figure that the output voltage increases sharply in the high frequency region, causing significant ringing [See the upper trace in (a).] in the output voltage waveform in response to the pulsed light input. This gain operates in the same manner with respect to operational amplifier input noise and may result in abnormally high noise levels. [See the upper trace in (c).]

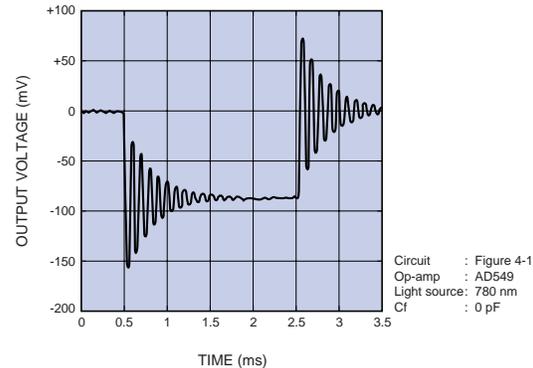
This occurs at the high frequency region when the reactance of the input capacitance and the feedback capacitance of the operational amplifier circuit jointly form an unstable amplifier with respect to input amplifier noise. In such a case, loss of measurement accuracy may result.

Figure 4-2 Gain peaking

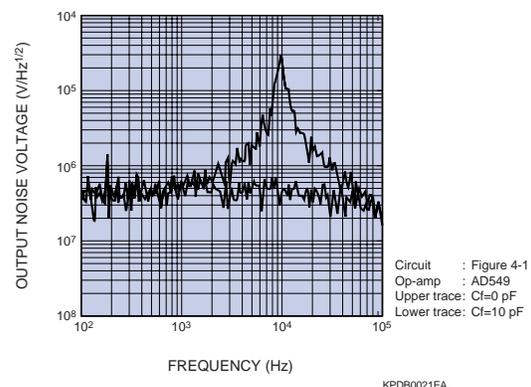
(a) Frequency response



(b) Light pulse response



(c) Frequency response of noise output



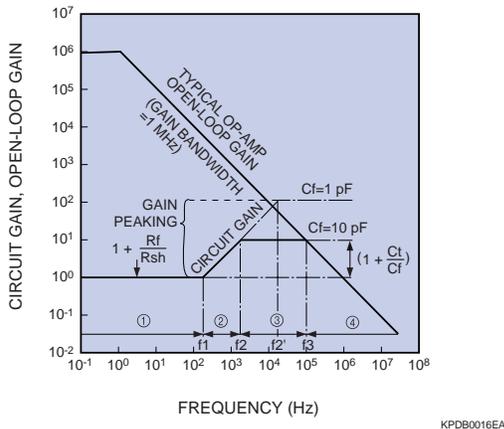
4-4. Gain peaking elimination

To achieve a wide frequency characteristic without gain peaking and ringing phenomena, it is necessary to select the optimum relationship between the photodiode, operational amplifier and feedback element. It will prove effective in the case of photodiodes to reduce the terminal capacitance C_t , as was previously explained in the section on Response speed and frequency response. In the operational amplifier, the higher the speed and the wider the bandwidth, the less the gain peaking that occurs. However, if adequate internal phase compensation is not provided, oscillation may be generated as a result. A feedback element, not only the resistance but also the feedback capacitance

should be connected in parallel, as explained previously, in order to avoid gain peaking. The gain peaking phenomena can be explained as follows, using the circuit shown in Figure 4-1. As shown in Figure 4-3, the circuit gain of the operational amplifier is determined for the low-frequency region ① simply by the resistance ratio of R_{sh} to R_f . From the frequency $f_1 = \frac{R_{sh} + R_f}{2 \pi R_{sh} R_f (C_f + C_t)}$ gain begins to increase with frequency as shown in region ②.

Next, at the frequency $f_2 = \frac{1}{2 \pi C_f R_f}$ and above, the circuit gain of the operational amplifier enters a flat region (region ③) which is determined by the ratio of C_t and C_f . At the point where frequency f_3 intersects the open-loop gain response at rolloff (6 dB/octave) of the operational amplifier, region ④ is entered. In this example, f_1 and f_2 correspond to 160 Hz and 1.6 kHz respectively under the conditions of Figure 4-1. If C_f is made 1 pF, f_2 shifts to f_2' and circuit gain increases further. What should be noted here is that, since the setting of increasing circuit gain in region ③ exceeds the open-loop gain curve, region ③ actually does not exist. As a result, ringing occurs in the pulsed light response of the operational amplifier circuit, and the gain peaking occurs in the frequency, then instability results. (See Figure 4-2.)

Figure 4-3 Graphical representation of gain peaking



To summarize the above points:

- a) When designing R_f and C_f , f_2 should be set to a value such that region ③ in Figure 4-3 exists.
- b) When f_2 is positioned to the right of the open-loop gain line of the operational amplifier, use the operational amplifier which has a high frequency at which the gain becomes 1 (unity gain bandwidth), and set region ③.

The above measures should reduce or prevent ringing. However, in the high-frequency region ③, circuit gain is present, and the input noise of the operational amplifier and feedback resistance noise are not reduced, but rather, depending on the circumstances, may even be amplified and appear in the output. The following method can be used to prevent this situation.

- c) Replace a photodiode with a low C_t value. In the example shown in the figure, $(1 + \frac{C_t}{C_f})$ should be close to 1.

Using the above procedures, the S/N deterioration caused by ringing and gain peaking can usually be solved. However, regardless of the above measures, if load capacitance from several hundred pF to several nF or more, for example, a coaxial cable of several meters or more and a capacitor is connected to the operational amplifier output, oscillation may occur in some types of operational amplifiers. Thus the capacitance load must be set as small as possible.

5. Si APD

5-1. Advantage of APD

When using an opto-semiconductor for low-light-level measurement, it is necessary to take overall performance into account, including not only the opto-semiconductor characteristics but also the readout circuit (operational amplifier, etc.) noise.

When a Si photodiode is used as a photodetector, the lowest detection limit is usually determined by the readout circuit noise because photodiode noise level is very low. This tendency becomes more obvious when the higher frequency of signal to be detected.

This is because the high-speed readout circuit usually exhibits larger noise, resulting in a predominant source of noise in the entire circuit system.

In such cases, if the detector itself has an internal gain mechanism and if the output signal from the detector is thus adequately amplified, the readout circuit can be operated so that its noise contribution is minimized to levels equal to one divided by gain (1/10 th to 1/100 th).

In this way, when the lowest detection limit is determined by the readout circuit, use of an APD offers the advantage that the lowest detection limit can be improved by the APD gain factor to a level 1/10 th to 1/100 th of the lowest detection limit obtained with normal photodiodes.

5-2. Noise characteristic of APD

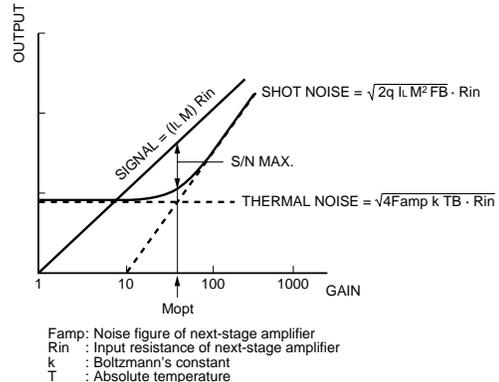
When the signal is amplified, the inherent excess noise resulting from statistical current fluctuation current fluctuation in the avalanche multiplication process is also generated. This noise current can be expressed by the following equation:

$$i_n = \sqrt{2 q I_L M^2 F B} \dots\dots\dots (5-1)$$

In the range of $M=10$ to 100 , F is approximated M^x .
 (F: Excess noise factor, M: Gain, I_L : Photocurrent at $M=1$,
 q: Electron charge, B: Bandwidth, x: Excess noise index)

In PIN photodiodes, using a large load resistance is not practical since it limits the response speed, so the circuit noise is usually dominated by the thermal noise of the photodiode. In contrast, the gain of an APD, which is internally amplified, can be increased until the shot noise reaches the same level as the thermal noise. The APD can therefore offer an improved S/N without impairing the response speed.

Figure 5-1 Noise characteristic of APD



Famp: Noise figure of next-stage amplifier
 Rin : Input resistance of next-stage amplifier
 k : Boltzmann's constant
 T : Absolute temperature

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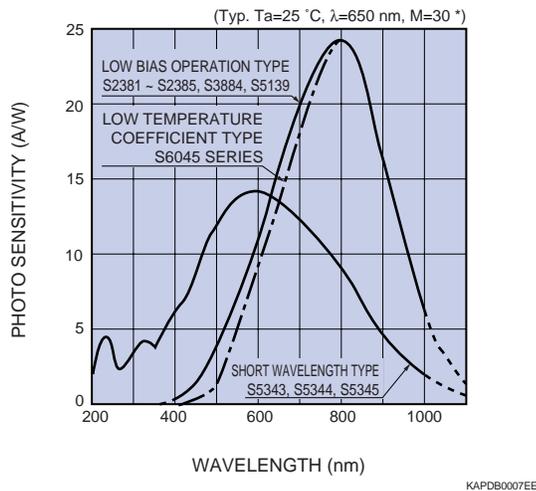
5-3. Spectral response of APD

The spectral response characteristics of the APD are almost the same as those of normal photodiodes if a bias voltage is not applied. When a bias voltage is applied, the spectral response curve will change. This means that the gain changes depending on the incident light wavelength. This is because the penetration depth of light into the silicon substrate depends on the wavelength so that the wavelength absorption efficiency in the light absorption region differs depending on the APD structure. It is therefore important to select a suitable APD.

To allow selection of spectral response characteristics, Hamamatsu provides two types of Si APDs: S2381 series and S6045 series for near infrared detection and S5343 series for light detection at shorter wavelengths.

Figure 5-2 shows typical spectral response characteristics measured with a gain of 30 at 650 nm wavelength.

Figure 5-2 Spectral response

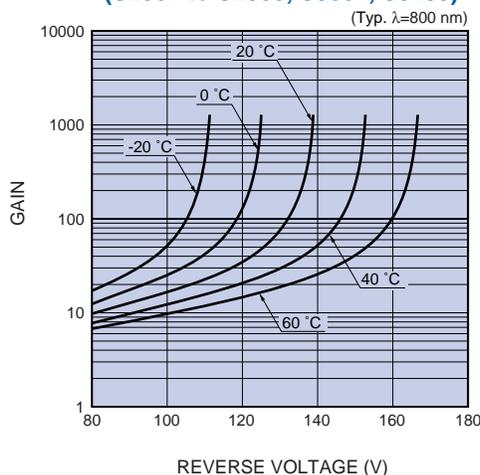


5-4. Temperature characteristic of gain

APD gain varies with temperature. For example, when an APD is operated at a constant bias voltage, the gain decreases with increasing temperature. Therefore, in order to obtain a constant output, it is necessary to vary the bias voltage according to the APD temperature or to keep the APD at a constant temperature. In S2381 series, the temperature coefficient of the bias voltage is nearly equal to that of the breakdown voltage which is 0.65 V/°C Typ. at a gain of 100.

Hamamatsu also provides S6045 series APDs which are designed to have an improved temperature coefficient (0.4 V/°C Typ.).

Figure 5-3 Gain temperature characteristics (S2381 to S2385, S3884, S5139)

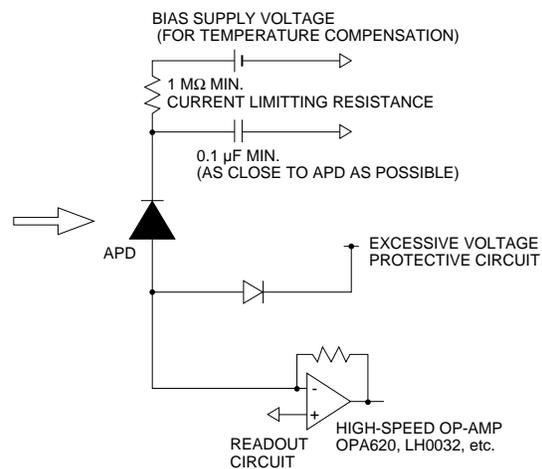


5-5. Connection to peripheral circuits

APDs can be handled in the same manner as normal photodiodes except that a high bias voltage is required. However the following precautions should be taken because APDs have an internal gain mechanism and are operated at a high voltage.

- 1) APDs consume a considerably large amount of power during operation, which is given by the product of the signal power \times sensitivity (e.g. 0.5 A/W at 800 nm) \times gain \times bias voltage. To deal with this, a protective resistor should be added to the bias circuit or a current limiting circuit should be used.
- 2) A low-noise readout circuit usually has a high impedance, so if an excessive voltage higher than the supply voltage for the readout circuit flows into the readout circuit, the first stage tends to be damaged. To prevent this, a protective circuit (diode) should be connected so that excessive voltage is diverted to the power supply voltage line.
- 3) As stated above, APD gain depends on temperature. The S2381 series has a typical temperature coefficient of 0.65 V/°C, but there is no problem with using the APD at a gain of around $M=30$ and $25^\circ\text{C} \pm 3^\circ\text{C}$. However, when used at a higher gain or wider temperature range, it is necessary to use some kind of temperature offset (to control the bias voltage according to temperature) or temperature control (to maintain the APD at a constant temperature).
- 4) When detecting low-level light signals, the detection limit can be determined by the shot noise of background light. If background light enters the APD, then the S/N may deteriorate due to the shot noise. As a countermeasure for minimizing background light, use of an optical filter, improving laser modulation or restricting the field of view is necessary.

Figure 5-4 Peripheral circuit example of APD



Reliability

If used within the specified operating ratings, chips of photodiodes will exhibit virtually no deterioration of characteristics. Deterioration can often be attributed to package, lead or filter failure. Package leakage at high temperatures and humidity, in particular, often causes the dark current to increase. Therefore, plastic and ceramic package photodiodes have a somewhat limited temperature and humidity range. In contrast, metal package types feature excellent resistance to ambient humidity. Photodiodes with filters are greatly affected by endurance of the filter to environmental conditions.

These factors must be taken into consideration when using and storing photodiodes. Hamamatsu photodiodes are subjected to reliable test based on JEITA (Japan Electronic Information and Technology Association). Reliable tests are also performed in compliance with MIL (US Military) standards and IEC (International Electrotechnical Commission) standards according to the product applications. The major reliability test standards used by Hamamatsu are summarized below in major reliability test standards.

Major reliability test standards

Test item	Condition	ED-4701	Criteria
Terminal strength	Pulling 10 seconds, bending 90° two times	A-111	Damage to terminal, etc.
Vibration	100 to 2000 Hz, 200 m/s ² XYZ directions, 4 minutes, 4 times each (total 48 minutes)	A-121	Appearance and electrical characteristics
Shock	1000 m/s ² , 6 ms XYZ directions, 3 times each	A-122	
Solderability	235 ± 5 °C, 5 or 2 seconds, 1 to 1.5 mm	A-131	Solderability
Resistance to soldering heat (except surface mount type)	260 ± 5 °C, 10 seconds, 1 to 1.5 mm	A-132	Appearance and electrical characteristics
Resistance to soldering heat (surface mount type)	Reflow 235 °C, 10 seconds	A-133	
High temperature storage	Tstg (Max.) : 1000 hours	B-111	
Low temperature storage	Tstg (Min.) : 1000 hours	B-112	
High temperature, high humidity storage	60 °C, 90 %: 1000 hours	B-121	
Temperature cycle	Tstg Min. to Tstg Max., in air, 30 minutes each, 10 cycles	B-131	
Electrostatic discharge	R=1.5 kΩ, C=100 pF, E=±1000 V, 3 times	C-111	
Resistance to solvent	Isopropyl alcohol, 23 ± 5 °C, 5 minutes	C-121	
High temperature reverse bias	ToPr Max., VR Max.: 1000 hours	D-212	Appearance and electrical characteristics

Note 1) Reference standards

Test method: JEITA-ED-4701 "Environmental and endurance test methods for semiconductor devices"

Note 2) Breakdown criteria standards

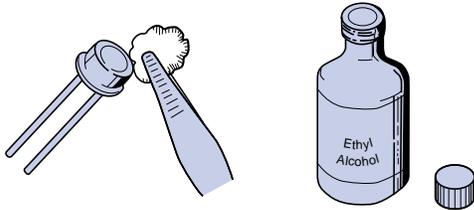
Test conditions and breakdown criteria standards table for collecting reliability test data (National Institute of Advanced Industrial Science and Technology)

Precaution for use

● Window

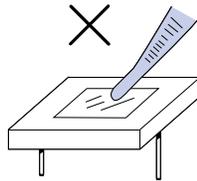
Care should be taken not to touch the window with bare hands, especially in the case of ultraviolet detection since foreign materials on the window can seriously affect transmittance in the ultraviolet range. (There have been occasions where contamination of the window by oil from hands reduced sensitivity at 250 nm by as much as 30 %.) If the window needs to be cleaned, use ethyl alcohol and wipe off the window gently. Avoid using any other organic solvents than ethyl alcohol as they may cause deterioration of the device's resin coating or filter.

When using tweezers or other hard tools, be careful not to allow the tip or any sharp objects to touch the window surface. If the window is scratched or damaged, accurate measurement cannot be expected when detecting a small light spot. In particular, use sufficient care when handling resin-coated or resin-molded devices.



Lightly wipe dirt of the window using ethyl alcohol.

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Avoid scratching the light input window with pointed objects (tweezers tip, etc.) or rubbing it with a hard flat surface.

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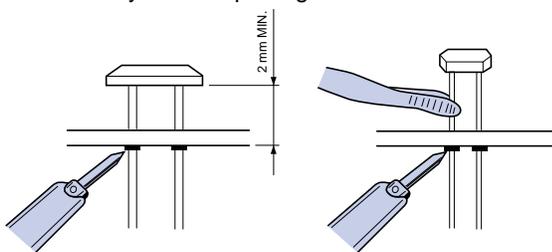
● Lead forming

When forming leads, care should be taken to keep the recommended mechanical stress limits: 5 N pull for 5 seconds maximum, two 90 degrees bends and two twists of the leads at 6 mm minimum away from the package base.

To form the leads of plastic-molded package devices, use long-nose pliers to hold near by the root of the leads securely.

● Soldering

Since photodiodes are subject to damage by excessive heat, sufficient care must be given to soldering temperature and dwell time. As a guide, metal package devices should be soldered at 260 °C or below within 10 seconds, ceramic package devices at 260 °C within 5 seconds at 2 mm minimum away from the package base, and plastic package devices at 230 °C or below within 5 seconds at 1 mm minimum away from the package base.



Mount ceramic package types 2 mm minimum away from any surface and solder at 260 °C maximum for 5 seconds maximum time.

Use tweezers, etc. as a heatsink when soldering small photodiodes.

KPDC0013EB

● Recommended soldering condition

Package	Soldering temperature Max. (°C)	Soldering time Max. (s)	Remark
Metal	260	10	
Ceramic	260	5	2 mm or more away from package
Ceramic chip carrier	260	5	S5106, S5107 non moisture absorption
Plastic	230	5	1 mm or more away from package

● Cleaning

Use alcohol to remove solder flux. Never use other type of solvent because, in particular, plastic packages may be damaged. It is recommended that the device be dipped into alcohol for cleaning. Ultrasonic cleaning and vapor cleaning may cause fatal damage to some types of devices (especially, hollow packages and devices with filters). Confirm in advance that there is no problem with such cleaning methods, then perform cleaning.

Some caution may be needed when using the photodiode according to the particular structure. Cautions needed when using various products are listed on the next page.

Bare chip Si photodiode (S3590-19, S6337-01)

S3590-19 and S6337-01 have a windowless package and does not incorporate measures to protect the photodiode chip.

- Never touch the photodiode chip surface or wiring.
- Wear dust-proof gloves and a dust-proof mask.
- Use air-blow to remove foreign objects or objects attached to the surface.
- Do not attempt to wash.

Si photodiode with preamp

The Si photodiode with preamp is prone to damage or deterioration from static electricity in the human body, surge voltages from test equipment, leakage voltage from soldering irons, and packing materials, etc.

To eliminate the risk of damage from static electricity, the device, worker, work location, and tool jig must all be at the same electrical potential. Take the following precautions during use.

- Use items such as a wrist strap to get a high resistance (1 M Ω) between the human body and ground to prevent damage to the device from static electricity that accumulates on the worker and the worker's clothes.
- Lay a semi-conductive sheet (1 M Ω to 100 M Ω) on the floor and also on the workbench, and then connect them to ground.
- Use a soldering iron having an insulation resistance of 10 M Ω or more and connect it to ground.
- Conductive material or aluminum foil is recommended for use as a container for shipping or packing. To prevent accumulation of static charges, use material with a resistance of 0.1 M Ω /cm² to 1 G Ω /cm².
- If electric current or voltage is applied in reverse polarity to an electronic device such as a preamplifier, this can degrade device performance or destroy the device. Always check the wiring and dimensional diagram to avoid misconnection.

Surface mount type Si photodiode

Surface mount Si photodiodes come in ceramic or plastic package types. Sealing resin used for photodiodes was designed with light transmittance in mind and so has low resistance to moisture and heat compared to sealing resin for general-purpose IC. This means that special care is required during handling. Unexpected troubles can occur if the IC temperature profile is used in reflow soldering. Therefore keep the following points in mind.

1) Ceramic type (silicone resin coating type)

- The resin protecting the photodiode surface is soft so that applying an external force may damage the resin surface, warp the bonding wires, or break wires, so avoid touching the surface as much as possible.
- If stored for 3 months while unpacked or if more than 24 hours have elapsed after unpacking, bake for 3 to 5 hours at 150 °C in a nitrogen atmosphere, or for 12 to 15 hours at 120 °C in a nitrogen atmosphere.
Note) Stick materials are vulnerable to heat, so do not try baking while the photodiodes are still in a stick.

2) Plastic type (epoxy resin mold type)

- Trouble during reflow is due to moisture absorption in the epoxy resin forming the package material. During soldering, the amount of moisture increases suddenly due to the heat and trouble such as peeling on the chip surface and package cracks is prone to occur.
- The packing is not usually moisture-proof so baking for 3 to 5 hours at 150 °C or for 12 to 15 hours at 120 °C in a nitrogen atmosphere is necessary before reflow soldering.
Note) Stick materials are vulnerable to heat, so do not try baking while the photodiodes are still in a stick.
- When required, it is possible to bake photodiodes prior to shipping and pack them in a moisture-proof case.

3) Reflow soldering

- Reflow soldering conditions depend on factors such as the PC board, reflow oven and product being used. Please ask in advance, about recommended reflow conditions for a particular product.

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